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Rec'd PCT/PTO 15 APR 2002

**BERESKIN & PARR**

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FORM PTO-1390 (REV. 9-2001)		U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE	ATTORNEY'S DOCKET NUMBER <b>11035-46</b>
<b>TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371</b>			U.S. APPLICATION NO. (If known, see 37 CFR 1.5) <b>10/089100</b>
INTERNATIONAL APPLICATION NO. <b>PCT/CA00/01183</b>	INTERNATIONAL FILING DATE <b>October 13, 2000</b>	PRIORITY DATE CLAIMED <b>October 15, 1999</b>	
TITLE OF INVENTION <b>METHOD AND APPARATUS FOR DELIVERING POWER TO A MECHANICAL OR ELECTRIC</b>			
APPLICANT(S) FOR DO/EO/US <b>Conrad</b>			
Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:			
1. <input checked="" type="checkbox"/> This is a <b>FIRST</b> submission of items concerning a filing under 35 U.S.C. 371. 2. <input type="checkbox"/> This is a <b>SECOND</b> or <b>SUBSEQUENT</b> submission of items concerning a filing under 35 U.S.C. 371. 3. <input checked="" type="checkbox"/> This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (21) indicated below. 4. <input type="checkbox"/> The US has been elected by the expiration of 19 months from the priority date (Article 31). 5. <input checked="" type="checkbox"/> A copy of the International Application as filed (35 U.S.C. 371(c)(2)) a. <input type="checkbox"/> is attached hereto (required only if not communicated by the International Bureau). b. <input checked="" type="checkbox"/> has been communicated by the International Bureau. c. <input type="checkbox"/> is not required, as the application was filed in the United States Receiving Office (RO/US). 6. <input type="checkbox"/> An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)). a. <input type="checkbox"/> is attached hereto. b. <input type="checkbox"/> has been previously submitted under 35 U.S.C. 154(d)(4). 7. <input checked="" type="checkbox"/> Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)) a. <input checked="" type="checkbox"/> are attached hereto (required only if not communicated by the International Bureau). b. <input type="checkbox"/> have been communicated by the International Bureau. c. <input type="checkbox"/> have not been made; however, the time limit for making such amendments has NOT expired. d. <input type="checkbox"/> have not been made and will not be made. 8. <input type="checkbox"/> An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371 (c)(3)) 9. <input type="checkbox"/> An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)). 10. <input type="checkbox"/> An English language translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)). <b>Items 11 to 20 below concern document(s) or information included:</b> 11. <input type="checkbox"/> An Information Disclosure Statement under 37 CFR 1.97 and 1.98. 12. <input type="checkbox"/> An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included. 13. <input checked="" type="checkbox"/> A <b>FIRST</b> preliminary amendment. 14. <input type="checkbox"/> A <b>SECOND</b> or <b>SUBSEQUENT</b> preliminary amendment. 15. <input type="checkbox"/> A substitute specification. 16. <input type="checkbox"/> A change of power of attorney and/or address letter. 17. <input type="checkbox"/> A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 - 1.825. 18. <input type="checkbox"/> A second copy of the published international application under 35 U.S.C. 154(d)(4) 19. <input type="checkbox"/> A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4) 20. <input type="checkbox"/> Other items or information:			

BERESKIN &amp; PARR

JC13 Rec'd PCT/PTO 15 APR 2002

U.S. APPLICATION NO. (37 CFR 1.53) n/a <b>10/089100</b>		INTERNATIONAL APPLICATION NO. PCT/CA00/01183		ATTORNEY'S DOCKET NUMBER 11035-46	
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21. <input checked="" type="checkbox"/> The following fees are submitted <b>BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)):</b> Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO. . . . . \$1040.00  International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO . . . . . \$890.00  International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO . . . . . \$740.00  International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4) . . . . . \$710.00  International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) . . . . . \$100.00 <b>ENTER APPROPRIATE BASIC FEE AMOUNT =</b>				<b>CALCULATIONS PTO USE ONLY</b>          <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; text-align: right;">\$</td> <td style="width: 50%; text-align: center;">890.00</td> </tr> <tr> <td style="text-align: right;">\$</td> <td style="text-align: center;">130.00</td> </tr> </table>		\$	890.00	\$	130.00
\$	890.00								
\$	130.00								
Surcharge of \$130.00 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input checked="" type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(e)).				\$ 130.00					
CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE						
Total claims	37 - 20 =	17	x \$18.00	\$ 306.00					
Independent claims	7 - 3 =	4	x \$84.00	\$ 336.00					
MULTIPLE DEPENDENT CLAIM(S) (if applicable)				+ \$280.00	\$				
<b>TOTAL OF ABOVE CALCULATIONS =</b>				\$ 1,662.00					
<input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2.				\$					
<b>SUBTOTAL =</b>				\$ 1,662.00					
Processing fee of \$130.00 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				\$					
<b>TOTAL NATIONAL FEE =</b>				\$ 1,662.00					
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property +				\$					
<b>TOTAL FEES ENCLOSED =</b>				\$ 1,662.00					
				Amount to be refunded:	\$				
				charged:	\$				

a. ☒ A check in the amount of \$ 1,662.00 to cover the above fees is enclosed.

b. ☐ Please charge my Deposit Account No. \_\_\_\_\_ in the amount of \$ \_\_\_\_\_ to cover the above fees. A duplicate copy of this sheet is enclosed.

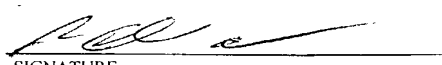
c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 022095. A duplicate copy of this sheet is enclosed.

d. ☐ Fees are to be charged to a credit card. **WARNING:** Information on this form may become public. **Credit card information should not be included on this form.** Provide credit card information and authorization on PTO-2038.

**NOTE:** Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO

**Bereskin & Parr**  
 Box 401, 40 King Street West  
 Toronto, Ontario Canada M5H 3Y2

  
 SIGNATURE  
 Philip C. Mendes da Costa  
 NAME  
 33,106  
 REGISTRATION NUMBER

Barristers and Solicitors/Patent and Trade Mark Agents  
Practice Restricted to Intellectual Property Law

April 12, 2002

Philip C. Mendes da Costa  
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Your Reference: N/A  
Our Reference: 11035-46/PMdC

**PRELIMINARY AMENDMENT**

The Commissioner of Patents  
& Trademarks  
Washington, D.C.  
U.S.A. 20231

Dear Sir:

**Re: National Phase Entry of PCT/CA00/01183**  
**Title: METHOD AND APPARATUS FOR DELIVERING POWER TO**  
**A MECHANICAL OR ELECTRICAL SYSTEM**  
**Applicant: Conrad**

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Please amend the application as follows:

**In the Specification:**

Please insert before the heading "FIELD OF THE INVENTION" the following:--This application is a continuation of United States Patent Number 6,307,358.--.

**In the Claims**

Please amend claims 16, 17 and 37 as follows:

16. The method as claimed in claim 1 wherein the load comprises a battery in which, during the discharge of the battery, chemical reactions occur that can utilize electrons having differing potentials and during recharging, the chemical reactions are reversed and the pulse train is modulated to preferentially use electrons having a higher potential to reverse chemical reactions requiring higher potential electrons.

17. The method as claimed in claim 1 wherein the load comprises a battery in which, during the discharge of the battery, chemical reactions occur that can utilize electrons having differing potentials and during discharging the pulse train is modulated to preferentially use higher potential electrons to provide energy to an external load.

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37. A method for charging a battery comprising providing an electrical signal to reverse chemical reactions which occur during the discharge of the battery wherein different chemical reactions can utilize electrons having differing potentials and modulating the signal to preferentially use electrons having a higher potential to reverse chemical reactions requiring higher potential electrons.

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**Remarks**

This preliminary amendment is filed together with the National Phase Entry of PCT Application PCT/CA00/01183. During the prosecution of the PCT application, the claims were amended. By this Preliminary Amendment, the applicant has amended three of the claims.

Attached hereto is a marked-up version of the changes made to the specification and claims by the current amendment. The attached page is captioned **"Version with markings to show changes made."**

Applicant respectfully requests that a timely Notice of Allowance be issued in this case.

Yours truly,



Philip C. Mendes da Costa

Registration No. 33,106

/kp

Encl.

**VERSION WITH MARKINGS TO SHOW CHANGES MADE**

16. The method as claimed in claim 1 wherein the load comprises a ~~rechargeable~~ battery in which, during the discharge of the battery, chemical reactions occur that can utilize electrons having differing potentials and during recharging, the chemical reactions are reversed and the pulse train is modulated to preferentially use electrons having a higher potential to reverse chemical reactions requiring higher potential electrons.

17. The method as claimed in claim 1 wherein the load comprises a ~~rechargeable~~ battery in which, during the discharge of the battery, chemical reactions occur that can utilize electrons having differing potentials and during discharging the pulse train is modulated to preferentially use higher potential electrons to provide energy to an external load.

37. A method for charging a ~~rechargeable~~ battery comprising providing an electrical signal to reverse chemical reactions which occur during the discharge of the battery wherein different chemical reactions can utilize electrons having differing potentials and modulating the signal to preferentially use electrons having a higher potential to reverse chemical reactions requiring higher potential electrons.

Title: METHOD AND APPARATUS FOR DELIVERING POWER TO A MECHANICAL OR ELECTRICAL SYSTEM

FIELD OF THE INVENTION

5                   This invention relates to power control systems and methods of delivering power to a mechanical or a fluid mechanical system. In particular, this invention relates to the use of impulsed power.

10   BACKGROUND OF THE INVENTION

                  Power control systems are used to control the rate of delivery of power to a member which requires power or which performs work. For example, power control systems are used to control the delivery of electrical power to a load (eg. a motor or other  
15   electromechanical devices which produce work such as solenoids, loudspeakers, florescent lights, incandescent lights and sodium lamps). The load may also be a battery wherein the power control system is used to control the charging and/or the discharging of the battery. Power control systems are also used in mechanical systems such as to  
20   control the delivery of power from an internal combustion engine. Examples of power control systems for such mechanical systems include governors and regulators for power generators.

                  Historically, power control systems have been designed to provide a uniform flow of power. For example, in the case of electrical  
25   motors, power delivery systems have been developed so as to ensure a continuous flow of electricity to a motor so that the drive shaft driven by the motor runs at a constant rate of revolution. In this way, the motor operates smoothly (i.e. without any vibrations). Similarly, even in mechanical systems, such as the use of an internal combustion  
30   engine to drive a vehicle (e.g. a car, train, airplane or the like), the power control systems have been developed so as to ensure that the engine provides smooth acceleration to the vehicle.

                  More recently, developments have been directed also towards decreasing the power requirements of a system. Typically,

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such work has been developed to reduce the actual amount of power required to operate the system while still maintaining a uniform flow of power. Examples of such developments include improved laminations and wiring for motors and generators to reduce power  
5 lost as heat.

There are also many applications wherein no power control system is utilized. An example of this is lighting. Fundamentally, an incandescent light bulb has a filament, usually contained within a glass enclosure, filled with a gas selected to  
10 maximize filament life. In use, an electric current is passed through the filament and simply serves to heat the filament to a very high temperature. The effect of this is to cause the filament to radiate electromagnetic radiation. It is well known that the spectrum of radiation produced is dependent upon the temperature of the  
15 filament. The filament is designed to reach temperatures such that a significant proportion of the radiation falls within the visible band of the electromagnetic spectrum. Unfortunately, the electromagnetic spectrum produced by a heated object, such as a filament, is necessarily broad, and much of the radiation falls either in the infrared or  
20 ultraviolet bands. This is highly undesirable. However, conventionally, it has simply been accepted that the physics of radiation or a heated body necessarily determines characteristic. Accordingly, this is simply accepted, and common incandescent light bulbs have a relatively low efficiency.

25 Similarly, a fluorescent light bulb typically has a gas, eg. mercury vapour, contained within a glass enclosure. In use, an electric current is passed through the mercury vapour to ionize the vapour. This in turn excites a fluorescent coating on the glass, to produce visible light as well as electromagnetic radiation outside the visible  
30 spectrum.



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Another example are electric motors and other devices which are powered by batteries or cells. Batteries or cells are commonly classified into two types, namely: primary cells, which are single use cells and, after discharge, cannot be recharged for further use; and  
5 secondary cells or batteries, which are subjected to a large number of charge and discharge cycles. Commonly, the current or energy drain from a battery or cell, whether this be a primary cell or secondary cell, is determined solely by the characteristics of the load. While there are a number of concepts employing pulse width modulation which are  
10 used to control the power consumption of electric motors, these known techniques are directed solely to controlling the motor, without regard to the effect on the energy source, and in particular without regard to any impact on the drain from a battery source.

Secondary batteries or cells deliver a DC current.  
15 Accordingly, charging of such secondary cells is commonly done by connection to a suitable, fixed DC potential. Current flow into the cell is then determined by the electrical characteristics of the cell, including the internal resistance of the cell. Practically, when charging the cell, the current initially has a relatively high value, and then reduces  
20 down, in some approximate exponential fashion. When a secondary battery is recharged, heat is produced. This heat is a byproduct of the recharging process and constitutes a loss of energy when a battery or cell is recharged. The speed at which a secondary battery or cell can be recharged is generally governed by the temperature to which the  
25 battery may be raised without degradation of the battery occurring.

Despite the advances which have been made in recent years in power control systems, a need still exists to increase the energy efficiency of electrical and mechanical devices as well as the speed and efficiency of battery recharging.

30

#### **SUMMARY OF THE INVENTION**

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In the research which has been undertaken by the inventor, it has surprisingly been found that the objective of providing a uniform flow of power to a system results in inefficiencies. Various systems operate on a cyclical basis which is not uniform. In accordance to the instant invention, in order to increase the energy efficiency of a system, the power is provided to, or withdrawn from, the system so as to operate a system in a regime in which it operates more efficiently. These systems include transmitting motive force between a fluid and an apparatus (eg. a fan blade or turbine) positioned in the fluid flow path, the production of light and other forms of radiation (including in particular infrared and x-ray radiation) and the charging and discharging of batteries. In each of these systems, the input of power results in the creation of work (eg. a fluid is moved, radiation is produced, electricity is generated or a battery is charged). However, the systems perform more work than is required. For example, in the case of light bulbs, lights bulbs will emit light (visible radiation), as well as radiation in band widths which are not visible (ancillary work). By reducing the non-visible radiation emitted by a light bulb, the same amount of visible light may be produced using less power. By providing pulsed power to the system, the system may be driven to perform the required work (eg. the production of light) and at least a reduced amount of ancillary work (eg. the production of non-visible radiation).

In accordance with the instant invention, a method of controlling the electrical power applied to a load comprises the steps of producing a pulse train comprising a series of pulses defining a cycle in which a portion of the pulse train having a duration of 10% of the cycle delivers more than 20% of the total power to the load which the load receives each cycle, and, supplying the pulse train to the load to supply power to the load. Accordingly, a portion of pulse train having

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a duration of 10% or less of the time of a cycle deliveries 20% or more of the power.

In one embodiment, the method further comprises the step of providing an electric power supply and the pulse train is produced by modulating the electric power supply to produce the pulse train.

In accordance with another aspect of the instant invention, a method of controlling the mechanical power applied to a load, the method comprises the steps of producing changes in the acceleration of a mechanical member whereby a series of differing accelerations are applied in a repeating pattern to produce the mechanical power, a portion of the series having a duration of 10% of the pattern delivers more than 20% of the total power to the load which the load receives during the repetition of each period and, supplying the mechanical power to the load to supply mechanical power to the load.

In one embodiment, the load comprises an impact member and the mechanical power is modulated to reduce degradation of a Prandtl layer which forms on the Prandtl layer as fluid travels over the impact member.

In another embodiment, the mechanical member comprises an impact member and the mechanical power is modulated to reduce degradation of a Prandtl layer which forms on the Prandtl layer as fluid travels over the impact member.

Preferably, the portion provides 30% - 70%, more preferably 40 - 60% and most preferably 45% - 55% of the total power the load receives each second.

The frequency of the pulse train may vary from 6 - 20Hz and preferably 9 - 15 Hz. It will be appreciated that if mechanical power is being applied to a load, then the series of pulses are effectively applied in a cycle which is preferably of the same frequency as an

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electrical signal as taught herein. Further, each cycle may contain from 1 - 20, preferably 5 - 20, more preferably 5 - 15 and most preferably 9 - 13 pulses or differing accelerations. For example, the pulse train may be produced by providing a constant power supply to the load (eg. a constant DC or AC signal) and superimposing on the signal which is supplied to the load one or more pulses. Thus, if a single pulse is superimposed, the load will receive a signal providing a continuous power level and, once a cycle, a signal at a higher power level. Preferably, in the case of an electric signal, the increased power is provided by increasing the voltage of the signal supplied to the load. It will be appreciated that a power control system for a mechanical system may be operated in the same manner.

Further, it is also preferred that the signal is non-uniform. For example, the signal is not synchronized to occur at the same point in each rotation or series of rotations of the motor and hence is not designed to maintain a uniform angular velocity or uniform momentum or uniform power input or distribution.

Referring to Figure 1, a plurality of different wave forms are shown. These include DC (Figure 1a), AC (Figure 1b), pulsed DC (Figure 1c) and a pulse width modulated signal (Figure 1d). The power transfer spectrum of each of these signals is substantially uniform. By this, it is meant that over a given period of time, a relatively uniform amount of power is delivered by a signal to a load. In the case of DC, it is understood that a uniform amount of power is effectively continuously provided to a load. In the case of AC or pulsed DC power, over each cycle, the same amount of power is provided. For example, in the case of a 60 Hz signal, the same amount of power is provided each 1/60 of a second. The power transfer spectrum of a pulse width modulated system delivers substantially less than 20% of the power in 10% of the time. Therefore, measuring the cycle from one point to another, the same amount of power is provided during each cycle. A

pulse width modulated signal, if provided to a motor, typically provides power to the motor at the same point in each rotation. All of these signals are designed so that the output of a device driven by these signals appears to be constant. In contrast, a pulse string  
 5 according to the instant invention is shown in Figure 1(e). As can be seen, the amount of power which is provided per unit time is non-uniform. In particular, in this example, most (e.g. 50%) of the power delivered to a load is provided in 0.006 seconds and each cycle or period lasts .08 seconds. The output of a device driven by such a signal  
 10 does not appear to be constant. For example, in the case of a motor, a person may perceive vibrations produced by the operation of the motor.

There are many applications today in which electric motors are employed. The energy consumption of motors for  
 15 pumping gases and liquids accounts for over one-quarter of all electricity consumed in the world today. There are known a number of techniques employing pulse width modulation to control the power consumption of motors. Such techniques have had modest success and generally are provided to control motor power or speed with little  
 20 or no regard for improving motor efficiency. While the power is pulsed, the pulses are symmetrical (i.e. the pulses are designed to provide about the same amount of power so that the motor receives a uniform supply of power).

In accordance with the present invention, the power  
 25 consumption of electric motors, particularly in such applications as the movement of air and pumping of liquids is substantially reduced while still performing the same level of work. Research by the inventor has found that these types of electromechanical assemblies have a natural resonance. Additionally, it has been found that when  
 30 the electrical signal or power supplied to the device is conditioned, so as to provide energy in synchronism with natural resonant

In accordance with another aspect of this invention, the present inventor has realized is that both for charging and discharging a battery, conventional techniques lead to much wastage of energy. Conventionally, as noted above, both for charging and discharging,

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current is drawn off essentially as a constant DC current. For practical applications, discharging will often result in a varying or intermittent current; but the essentially DC nature of the discharge certainly does not amount to a pulsed discharge as taught by the present invention  
5 and as detailed below).

What the present inventor has realized is that, for both charging and discharging, one can identify an apparent resonant effect. At the atomic level, it is believed that charging and discharging essentially requires ionization (or the reverse) of individual atoms or  
10 molecules. If such ionization is effected by application of a constant DC potential, often ionization is effected at a less than optimum quantum state, thus requiring excess energy and wastage of energy. On the other hand, if ionization is, in effect, synchronized with an optimum quantum state of the particular atom or molecule, then less energy is  
15 required.

At a macroscopic level, the inventor has discovered that this appears as a resonant effect. Thus, for charging, the inventor has discovered that if the series or train of pulses is applied during the charging process, then much more efficient charging can be obtained.  
20 In effect, between each pulse, the battery or cell is permitted to relax, and when the next pulse is applied, atoms or molecules are in an optimum state for receiving a charge. It is possible to devise an optimum wave form, to increase or to optimize the power or energy output of primary and secondary batteries and energy input to  
25 secondary batteries. This is achieved by developing an algorithm relating the power or energy obtained from (or delivered to) the battery to key parameters of the pulse train, namely, voltage, frequency and pulse width. Then, one or more, and optionally two or more of these parameters (voltage, frequency and pulse width) are optimized for a  
30 particular load, to improve the performance of the battery during charging or discharging.

It will be appreciated that apparatus embodying this mode are also within the scope of this invention.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

5           These and other advantages of the instant invention will be more fully and particularly understood in connection with the following description of the preferred embodiments of the invention in which:

          Figure 1(a) - (d) are prior art electrical signals and Figure  
10   1(e) is an electrical signal according to the instant invention;

          Figure 2 is a schematic view of an internal combustion engine in accordance with the present invention.

          Figure 3 is a schematic view of an apparatus and an electric motor in accordance with the present invention;

15           Figure 4 is a circuit schematic which may be used with the apparatus of Figure 3;

          Figure 5 is a cross-section of a vacuum cleaner including the motor control circuit of Figure 4;

          Figure 6 is an alternate schematic view of an apparatus  
20   and an electric motor in accordance with the present invention;

          Figure 7 is an alternate schematic view of an apparatus and an light bulb in accordance with the present invention;

          Figure 8 is an alternate schematic view of an apparatus for discharging a battery in accordance with the present invention;

25           Figure 9 is an alternate schematic view of an apparatus for charging a battery in accordance with the present invention;

          Figure 10 is a graph of electrical power versus flow for a motor receiving a pulsed signal according to the instant invention;

30           Figure 11 is a graph of power versus flow for a second motor receiving a pulsed signal according to the instant invention;



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Figures 12(a) - (c) are a graph of voltage versus time and a graph of current versus time for a pulse train signal provided to a motor;

Figure 13 is a representation of a pulsed signal provided to a light bulb in accordance to the instant invention; and,

Figure 14 is a graph showing the voltage and current for an alternate pulsed signal provided a light bulb.

# DESCRIPTION OF THE PREFERRED EMBODIMENT

In one aspect, the invention relates to fluid mechanical systems. Fluid mechanical systems include those systems which use an impact member to transmit motive power between the impact member and the fluid. The impact member may be designed for transmitting motive power from the impact member to the fluid whereby the movement of the impact member causes the fluid to move. Examples of such systems are fans, pumps, turbines. These devices have impact members (eg. fan blades, propellers, turbine foils and the like) which interact with the fluid to produce movement of the fluid. The impact member may alternately be designed for receiving motive power from the fluid and transmitting the motive power to, eg., a drive rod on which the impact member is mounted whereby the movement of the fluid causes the impact member to move. Examples of such systems are electrical generators and a steam powered engine wherein a fluid is expanded through a turbine. In each case, the impact member, hereinafter referred to as a "vane" deflects the fluid (a gas or a liquid) to move the fluid downstream (eg. a pump) or deflection of the fluid provides motive power (such as in the case of a propeller) to a vehicle or the like to produce mechanical power (such as rotational power provided by a drive rod wherein the drive rod is rotated by rotation of the impact member) or electrical power (such as in the case of an electric generator).

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By way of example, as gas passes over a fan blade, a Prandtl layer forms along the fan blade. As a fan blade rotates, a thicker boundary layer will be developed. At some point, the layer of fluid travelling along with the blade will be of a sufficient thickness such that all or a portion of the boundary layer will separate from the blade. When this occurs, turbulence or vortical flow will occur. Without being limited by theory, it is believed that as a fan blade rotates either the Prandtl layer is thickening and then thinning when a portion of it breaks off, or, alternately, that a plurality of layers are forming on top of the Prandtl layer and that these outer layers break off periodically at a certain thickness. In either case, when a portion of the layer travelling with the blade breaks off, this disrupts the Prandtl layer. The existence of the Prandtl layer is required to assist a fan blade in transmitting motive force to the fluid or receiving motive force from the fluid. Therefore preventing degradation of the Prandtl layer (e.g. the collapse of the Prandtl layer due to the sudden thickening of the boundary layer or the delamination of all or a portion of the Prandtl layer) increases the efficiency of a fan blade.

In accordance to the instant invention, power is delivered to the fan blade so as to prevent the Prandtl layer from collapsing or delaminating. By maintaining an effective Prandtl layer on a blade for a greater period of time, more of the energy which is input into the system to cause the fan blade to rotate will be transmitted to the fluid passing over the blade. Accordingly, the pulse train is modulated to vary the acceleration (which may be a negative acceleration, i.e. a deceleration) of the impact member to reduce degradation of a Prandtl layer which forms on the impact member as the fluid travels over the impact member.

Conventionally, the cyclical thickening of the boundary layer on the fan blade occurs since the power is supplied uniformly to the fan blade (i.e. a fan blade rotates at essentially a constant rpm). In

This invention has particular applicability to vacuum cleaners. As such, a motor for a vacuum cleaner is attached to a fan, for drawing air through the vacuum cleaner, so as to produce the desired vacuum effect. What the inventor has realized is that if the signal supplied to the motor is configured so as to cause deceleration just prior to collapse or delamination of the Prandtl layer, and to accelerate shortly thereafter so as to rethicken or reestablish the Prandtl layer and prevent it from completely collapsing. Thus the Prandtl layer is reduced of thinned down as opposed to collapsing or delaminating. Further, the acceleration results in the Prandtl layer being built up faster. In effect, this reduces the vortex energy thrown off from the blade, and hence significantly reduces energy losses. Accordingly, the algorithm for the pulse train for a vacuum cleaner should be developed, with this in mind. This is done simply by running a series of tests or experiments on a complete vacuum cleaner, which will

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allow for any effects which will alter the power consumption of the motor.

It will similarly be appreciated that the same effect may be obtained in non-electrical (i.e. mechanical systems). Once again, the mechanical system (e.g. an internal combustion engine) will be operated such that, eg., the shaft on which an impact member, eg. a piston, is mounted does not rotate at a constant rate but is accelerated and decelerated in a similar manner as an electrically operated fan blade for a vacuum cleaner so as to prevent the collapse or delamination of the Prandtl layer. More preferably, the impact member is operated so as to maintain the Prandtl layer between predetermined minimum and maximum thicknesses so that the effectiveness of the impact member in transmitting motor force to a fluid is maintained at a relatively constant level, but the angular velocity of the impact member is not held constant.

Therefore, in one aspect of the invention, there is provided a method of moving a fluid using a impact member, the method comprises providing power to rotate the impact member and form a Prandtl layer of fluid on the impact member as the impact member moves and, varying the rate of rotation of the impact member to reduce the degradation of the Prandtl layer as the fluid travels over the impact member. The impact member may comprise the power transfer member of a fluid pump and the method further comprises driving the impact member to cause the fluid to flow.

Therefore, in another aspect of the invention, there is provided a method of generating power from a fluid using a impact member comprises providing fluid to rotate the impact member and form a Prandtl layer of fluid on the impact member as the impact member moves, the impact member being drivingly connected to an apparatus for producing power in response to the rotation of the impact member and, varying the rate of rotation of the impact

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member to reduce the degradation of the Prandtl layer as the fluid travels over the impact member. The apparatus may comprise an electrical generator and the method further comprises driving the generator to produce electrical current. Alternately, the apparatus may  
 5 comprise drive rod and the method further comprises driving the drive rod to obtain mechanical power.

Referring to Figure 2, a mechanical system for providing a pulsed system according to the instant invention is shown. In accordance with this system, an internal combustion engine comprises  
 10 at least one and preferably a plurality of pistons 180. Just one such piston is shown in Figure 2 and it is received in the bore 184 of a cylinder 182. A drive rod 186 is pivotally attached to piston 182. Drive rod 186 has a distal end 188 which may be drivingly connected to a crank shaft or other power transfer coupling known in the art of  
 15 internal combustion engines. Cylinder 182 is provided with first and second fuel dispensers 190 and 192, eg. fuel injectors. Each fuel dispenser is in fluid communication with a source of fuel, such as by means of a fuel line 194 which feeds individual fuel feed lines 196. A fuel ignition system, such as spark plug 198 is also provided. An  
 20 electronic ignition system 200 is provided to control fuel dispenser 190, spark plug 198 and fuel dispenser 192 by means of wires 202, 204 and 206 respectively.

First and second fuel dispensers 190 and 192 provide different aliquots of fuel to cylinder 182. For example, first fuel  
 25 dispenser 190 may be designed to provide one microliter of fuel to the cylinder whereas second fuel dispenser 192 may be designed to provide two microliters of fuel to cylinder 182. Moreover, the amount of fuel dispensed or injected or by each dispenser 190, 192 is preferably variable provided that differing amounts may be sequentially  
 30 introduced into bore 184 so as to provide differing levels of power as described herein. Further, a single dispenser or injector may be used

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for each cylinder 182 provided it is capable of providing differing quantities of fuel to bore 184. Electronic ignition system 200 may sequentially actuate one or the other, or both, fuel dispensers by means of wires 202 and 206. Spark plug 198 will cause ignition of the fuel in  
5 cylinder 182. By varying the amount of fuel which is ignited in cylinder 182, the amount of acceleration exerted on piston 182 by the ignition of the fuel is varied so as to provide the requisite pulsed acceleration to any member drivenly connected to drive rod 186. Thus, for example, drive rod 186 may be drivenly connected, by any means  
10 known in the art, to an impact member. Accordingly, the modulation of the fuel flow rate to the internal combustion engine and/or the spark temperature may be utilized to accelerate and decelerate the impact member so as to prevent, or at least reduce, the collapse or delamination of the Prandtl layer on the impact member. In particular,  
15 a reduced amount of fuel and/or a lesser spark would decelerate the crank shaft while extra fuel and/or a higher spark temperature would accelerate the crank shaft.

It will also be appreciated that the same operational mode may be utilized with impact members which interact with a fluid so as  
20 to cause the fluid to do work. Examples of these include turbine and windmills which are used to generate electricity. As a fluid (e.g. air or steam) passes over a foil or turbine, a Prandtl layer is built up which cyclically thickens and thins. By interacting with, e.g., the shaft on which the turbine is mounted so as to cause the turbine to accelerate  
25 and decelerate under the influence of the fluid (eg. using a solenoid to drive a brake member to periodically contact the shaft to slow the shaft or a clutch to selectively change the load on the shaft), the thickness of the boundary layer on the turbine may be controlled so as to prevent degradation of the Prandtl layer. In this way, a greater amount of  
30 power may be transmitted by the turbine from the fluid to a system (eg. an electrical generator or to a drive rod on which an impact member is

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attached so as to provide rotational mechanical power). It will be appreciated that, by accelerating and decelerating the turbine, the drive rod on which the impact member is mounted will provide non-uniform rotational power. This non-uniform rotational power may be converted to linear power or, alternately, to electrical current by means of an electrical generator. The electrical signal produced by the generator may accordingly be a pulsed signal which is the digital equivalent of the non-uniform rotational power fed to the generator. Such a signal may be provided to a load. Preferably, if the mechanical power is used to drive an electric generator and the pulsed signal produced by the generator would not cause the load to perform work in an energy efficient manner, the signal may be further attenuated so as to alter the pulse train produced by the generator to one which is appropriate for the load to which the generator is supplying power. In a similar manner, the non-uniform mechanical power provided by the drive rod may also be attenuated to provide continuous power or an alternate pulsed power which is appropriate for the system to which the drive rod provides power.

Alternately, the desired acceleration and deceleration of the impact member can be achieved by applying a pulse train signal to an electromagnetic clutch which couples a prime mover to the impact member. If the impact member is a fan blade or the like, then the prime mover is the shaft which is drivingly connected to the fan blade. If the impact member is a turbine for generating electricity, then the prime mover is the drive rod which is drivenly connected to the turbine. In the case of an electromagnetic clutch, the series of electrical pulses cause differential slip to occur in the clutch thereby accelerating and decelerating the impact member. A further alternative method produces the desired acceleration and deceleration of the impact member by applying a pulse train of hydraulic pressure pulses to a hydraulic mechanical clutch which couples a prime mover to the

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impact member. In the case of an hydraulic mechanical clutch, the series of pressure pulses cause differential slip to occur in the clutch thereby accelerating and decelerating the impact member.

5 In one embodiment, the electrical signal is used to power a fan blade, such as may be used in a vacuum cleaner. Figure 3 shows a voltage source 10, which can provide either AC or DC power, and connected to an electronic control unit 12 by connections or wires 13, 14. The electronic control unit 12 in turn is connected to the actual electric motor 15, by means of wires 16 and 17.

10 The electronic control unit 12 receives either an AC or DC power supply signal over the wires 13, 14. This is modified or conditioned by modulating the signal with a pulse train. The unit 12 effectively modifies one or more of the characteristics of the pulses, namely pulse width, voltage and frequency. This is done by  
15 modulating at least one, and possibly two or three of these characteristics. Thus, the unit 12 could modify: the pulse width and voltage of the signal; the frequency and voltage of the signal; the frequency and pulse width of the signal; or the frequency, pulse width and voltage together. Whichever characteristic is not modulated, is set  
20 at a fixed value.

For a given motor in a given system, the actual pulse train which is used will vary. A series of tests or experiments may be easily carried out to establish the characteristics that give optimum performance.

25 In order to optimize the performance of a given motor for a given load, a series of variables are sequentially altered and the power consumed is measured. For example, initially, the normal running voltage for the motor is applied and the frequency is increased in 10% increments. At each frequency increment, the pulse  
30 width of the signal is reduced until either the power consumed decreases by, eg., 25% or the motor r.p.m. is altered by more than 20%.



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This procedure is repeated for selected voltages, preferably 250% of the normal running voltage down to 20% of the normal running voltage such as by 10% decrements. When a voltage greater than the internal operating voltage is applied, the energy delivered in the pulses is kept  
5 to a level below the level at which degradation of the insulation by heat, or other physical damage will occur by reducing the duration (time) associated with the pulses. This data is then topographically mapped and an algorithm to optimize the motor is selected so as to reduce the power consumed by modulating the applied voltage,  
10 applied frequency and pulse width of the signal.

The pulse train comprises a set cycle of pulses, for example, a plurality of pulses that may be of the order of 10 pulses or more longer. Pulses within the cycle can vary, in terms of their pulse width and pulse height. This cycle is repeated continuously, to  
15 generate the pulse train.

Figure 4 shows a motor control circuit which may be used in a vacuum cleaner in accordance with the instant invention. Figure 5 exemplifies a vacuum cleaner including the circuit. As shown in Figure 5, an upright vacuum cleaner 70 has vacuum cleaner head 72  
20 and main casing 74. Cleaning head 72 has rear wheels 76 and front wheels 78 to enable movement of cleaning head 72 across a surface. Cleaning head 72 is provided with a rotatably mounted brush 80 which is positioned above air inlet 82. Cleaning head 72 has an air outlet 84 positioned at the end of air flow path 86. Rotatable valve 88 is  
25 provided in the cleaning head 72 so as to isolate the filtration means in main casing 72 from air flow path 86 when the vacuum cleaner is in the upright position shown in Figure 5.

Main casing 74 contains the filtration means which preferably comprises cyclone housing 90 defining cyclone chamber 92.  
30 Cyclone chamber 92 is provided with an air inlet 94 which is in air flow communication with air outlet 84 by means of air flow path 100.

Referring to Figure 4, power control circuit 112 comprises a motor controller as well as a battery charger. Battery 114 supplies 50% the power for motor 98 as DC current. The other half of the power is supplied to the motor through an inverter (namely field effect transistor 120 and transformer 122). This has the advantage that half the power is transmitted as DC (which has nominal circuit losses) and half is transmitted through the inverter (which may have an efficiency of eg. about 85%) for an overall efficiency of about 92.5%. It is recognized that by increasing the power channelled through the inverter, the flow rate of the mechanical system can be controlled.

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However, increasing the power channelled through the inverter increases the heat losses through the circuit and mitigates a portion of the energy saving realized in the fluid mechanical portion of the system. It will be appreciated the battery 114 may supply all of the power to motor 98 through the inverter circuit resulting in about a 7.5% reduction in the power savings. The instant design also advantageously allows multiple power levels to be supplied to motor 98.

The vacuum cleaner is operated by a user turning the vacuum cleaner on by an on/off switch 118, which may be any switch known in the art. When vacuum cleaner 70 is turned on, micro controller 116 receives a signal from switch 118 and in turn starts to oscillate field effect transistor 120 at a high frequency (e.g. about 60 KHz). Circuit 112 is provided with transformer 122 having primary and secondary coils 124 and 126. The high frequency oscillation produced by field effect transistor 120 causes primary coils 124 to induce a high voltage in secondary coils 126. The high voltage induced in second coil 126 is switched on and off by field effect transistor 128 at a much lower frequency (e.g. 9 Hz) as controlled by micro controller 116 by means of wire 152. The high voltage induced in second coil 126 may also be supplied to diode multiplier 172 which to provide current to, eg. an electrostatic generator in vacuum cleaner 70.

Field effect transistor 128 is connected to motor 98 via wire 130, switch 132 and wire 134. Accordingly, the pulse train developed by field effect transistor 128 is supplied to motor 98 so as to cause sub-rotational accelerations as described herein whereby the efficiency of the power transfer from motor 98 to the fluid stream passing through vacuum cleaner 70 is improved.

In a cyclonic vacuum cleaner, the impulses are preferably 1/81 seconds long having a voltage (amplitude) six times greater than the DC voltage supplied by battery 114 to motor 98 by means of wires

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136, 138. The frequency of the pulses produced by field effect transistor 128 is preferably 6-20 Hz for a cyclonic vacuum cleaner using a series universal motor wound to produce the desired flow rate when 50 volts AC is applied with 200 watts available. It will be appreciated that the pulse which is provided to motor 98 may be varied by changing the frequency of field effect transistor 128.

In accordance with another aspect of this invention, circuit 112 may include a microswitch 140 which is activated when vacuum cleaner 70 is placed in the upright position shown in Figure 5 (i.e. axis A of main casing 74 is essentially perpendicular to the surface being cleaned). Microswitch 140 may be of any known in the art which will provide a signal to microcontroller 116 depending upon the position of upper casing 74.

Microswitch 140 causes a signal to be sent to microcontroller 116 by means of wire 142. This causes microcontroller 116 to terminate the oscillation of field effect transistors 120 and 128 thereby reducing the power consumption and air flow through motor and fan blade assembly 98.

Typically, a user may leave a vacuum cleaner running when in the upright position when attending to other tasks associated with vacuuming such as to move furniture or other objects which may be in the way. When microswitch 140 is actuated, moving the vacuum cleaner into a standby mode, the power consumed by motor and fan blade assembly 98 is reduced thereby permitting a user to move furniture, answer the telephone or the like while reducing the power consumption of motor and fan blade assembly 98. Microswitch 140 may be utilized to switch a vacuum cleaner operating from a standard electrical outlet to a standby mode. This may be advantageous to decrease the noise produced by vacuum cleaner 70 when it is not being used. However, use of the standby mode is particular advantageous in a battery powered vacuum cleaner.

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Optionally, hose 102 is detachable from main casing 74 so as to enable above the floor cleaning, e.g. hose 102 may have a rigid wand 114 slidably received therein for receiving a crevice cleaning tool or other attachment. In such a case, circuit 112 preferably also includes microswitch 146 for switching motor and fan blade assembly 98 to a high flow mode. The higher flow is desirable for enhanced cleaning using accessory tools. Alternately, as the use of a hose causes additional pressure losses, increasing the power provided to motor and fan blade assembly 98 may result in the same flow rate when hose 102 is used. Microswitch 146 may be provided in the receptacle in which hose 102 is received and actuated when hose 102 is released from the receptacle (in the direction of arrow B). Microswitch 146 may be a pressure actuated switch (i.e. the switch may have a button which is pressed inwardly). When hose 102 is released, the button extends outwardly thereby sending a signal to microcontroller 116 by means of wire 148. In response to this signal, microcontroller 116 sends a signal to field effect transistors 120 and 128 by means of wires 150 and 152 respectively. This causes field effect transistor 120 to oscillate at a high frequency (e.g. 60 KHz or greater) and cause field effect transistor 128 to oscillate at a higher frequency than before (e.g. 11-15 Hz) with pulses of, e.g. 1/81 to 1/60 of a second for a typical cyclonic vacuum cleaner as described above. The longer pulse width and/or greater frequency of pulses delivered to motor and fan blade assembly 98 produces a higher flow of air through vacuum cleaner 70 than when the vacuum cleaner is drawing dirt laden air through inlet 82.

In accordance with another aspect of the instant invention, microcontroller 116 also includes a circuit for determining a level of charge remaining in battery 114. To this end, microcontroller 116 sends a signal to field effect transistor 120 which causes field effect transistor to switch on for a short period (e.g. approximately 0.1-0.2 seconds). This produces an impulse equivalent to DC. As the frequency

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of this impulse is very low, transformer 122 effectively becomes a low resistance short circuit across battery 114 thereby causing a current surge through low value resistor 154 which is series with transformer 122.

5                   The voltage drop across low value resistor 154 caused by the current surge is conducted to (e.g.) the analog to digital port of microcontroller 116 by means of wires 156 and 158. While the voltage which is supplied by battery 114 may be relatively constant over a substantial portion of the operating life of a battery (e.g. 75% or more),  
10 it has surprisingly been determined that the rate of rise of current in response to a momentary short circuit does not remain constant. In particular, as the capacity of the battery is reduced (i.e. charge is withdrawn from the battery), the ability of battery 114 to supply a current surge is also reduced. Therefore, it is possible to determine the  
15 capacity remaining in the battery by occasionally producing a short circuit across battery 114 and monitoring the rate of rise of the current in response to the short circuit. For a NiMH sub C battery pack comprising two sets of twelve sintered cells connected in parallel, the  $di/dt$  varies from 300 A/S to 120 A/S from 90% capacity to 20% capacity  
20 while the voltage output is essentially constant. Thus, by knowing the  $di/dt$  relationship for a battery over the capacity for a battery, microcontroller 116 may provide a signal indicating the amount of capacity remaining in the battery or, if the battery is being charged, the degree to which the battery has been charged.

25                   The same method may be utilized during the recharging of the battery to determine the charge state of the battery. Typically, the charge state of the battery is determined using the  $-\Delta V$ . When a battery is in the  $-\Delta V$  range, it is already overcharged. Rechargeable batteries are subject to degradation if their temperature increases too much, which  
30 occurs when they are overcharged. Therefore, it is advantageous to determine the charged state of a battery prior to the battery becoming

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overcharged. Accordingly, during the recharging of a battery, microcontroller 116 may cause field effect transformer 120 to occasionally emit a low frequency pulse thereby producing a current surge which may be measured by the voltage drop across low value resistor 154.

Preferably, microcontroller 116 includes means for opening the circuit to thereby shut off motor and fan blade assembly 98 when battery 114 is at a sufficiently low charge level. Accordingly, circuit 112 may shut down the power drawn from battery 114 by opening relay 160 which opens the circuit to motor and fan blade assembly 98 and by terminating the signals which are sent to field effect transistors 120 and 128.

It will be appreciated that battery 114 may be charged by removing battery 114 from vacuum cleaner 70 and placing it in a suitable charging unit. Preferably, battery 114 is charged in situ. To this end, vacuum cleaner 70 may include a plug 162 which is suitable for being received in a standard electrical outlet. Plug 162 is connected to circuit 112 by means of cord 164. When plug 162 is withdrawn from receptacle 166 (which may be provided at any desired position in vacuum cleaner 70), mechanical lever 168 trips switch 132 so as to disconnect motor and fan blade assembly 98 from the current. In this way, motor and fan blade assembly 98 will still receive current from wires 136 and 138 thereby causing motor and fan blade assembly 98 to operate at low power during the recharging operation. The operation of motor and fan blade assembly 98 at low voltage DC during the recharging operation causes motor and fan blade assembly 98 to operate at a low speed so that air may be drawn across battery 114 and over, e.g., heat sink 170 which is thermally connected to battery 114 so as to cool battery 114 while it is being charged. Optionally, switch 132 may be arranged to disconnect wire 136 from motor and fan blade assembly 98 so that motor and fan blade assembly 98 will not operate

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during the charging mode or to close another circuit to operate a cooling motor and fan assembly provided in air flow communication with battery 114 to reduce the sensible temperature of battery 114 during charging.

5 When plug 162 is removed from receptacle 166, a signal is sent to microcontroller 116 such that when plug 162 is plugged into a standard power outlet, field effect transistor 128 is operated at, e.g. 60 KHz by microcontroller 116 while field effect transistor 120 provides low frequency pulses (eg. 10 Hz) to charge battery 114. The frequency of  
10 operation of field effect transistor 128 can be raised or lowered to vary the output voltage used to charge battery 114.

The power control system may be designed to automatically optimize the power consumption of a system. Referring to Figure 6, the system of Figure 3 has added thereto a feedback system. In this  
15 embodiment, electronic control unit 12 is connected by wire 16 directly to a motor 15, and by wires 17 and 18 and an inductor 19, in series, to the motor 15.

A second inductor 20 is provided, inductively coupled to the inductor 19, and connected to a second electronic control unit 21 by wires  
20 22 and 23. The second electronic control unit 21 receives power through wires 30 and 31, connected to the first electronic control unit 12. Additionally, the second electronic control unit 21 provides control information, detailed below, to the first electronic control unit 12 through the wires 30', 31'.

25 To monitor the motor speed, a magnet 24 is mounted on the rotating shaft 25 of the motor, and is magnetically coupled to an inductor 26. The inductor 26 is connected by wires 27 and 28 to the second electronic control unit 21. Thus, rotation of the shaft 25 and the magnet 24 generate a pulse train from the inductor 26, which is detected by the  
30 second electronic control unit 21, and the frequency of this pulse train is proportional to the speed of the motor 15.



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A control input for the electronic control unit 21 is indicated schematically at 29. Although shown as a single lead, it will be understood that this could comprise a multiple lead input. It enables input of desired or intended characteristics for the motor  
5 behaviour, for example, speed and power supplied to the motor.

In use, the second electronic control unit 21 receives signals indicative of motor speed and current supplied to the motor. The control unit 21 is also pre-loaded with an algorithm relating motor performance to the three main parameters of a pulse train,  
10 namely frequency, pulse width and pulse height (or voltage). In dependence on this algorithm, sensed motor conditions or load and the input at 29, the electronic control unit 21 sends control signals to the first electronic control unit 12, to cause the control unit 12 to deliver a pulse train to the motor 15, which pulse train will give the  
15 desired motor performance.

In accordance with another aspect of the instant invention, the power control system is used in the management of power which is provided to a radiation emitting device such as an incandescent light bulb, a fluorescent light bulb and a sodium lamp. In  
20 all light emitting devices, electrical energy is input into the system to produce electrons having a higher electrical charge. These electrons are dynamically unstable and return to their natural orbital state. When this occurs, photons are emitted which result in the production of light. When energy is provided as a continuous signal to electrons, the  
25 electrons are raised to numerous quantum states. When the electrons release the additional energy imparted to them, they return to their natural orbital state and emit radiation. As the electrons are changing quantum states at essentially the same time, and as the release of energy from different quantum states produces a different  
30 wavelengths of radiation, the electrons, and accordingly the light emitting member, will emit a broad spectrum of radiation. An

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example of this are light bulbs which provide light not only in the visible spectrum but, in addition, light bulbs also emit radiation in other parts of the radiation spectrum including ultraviolet and infrared. In particular, the radiation emitting member (e.g. a filament  
5 in the case of an electric light bulb or the gas in the case of a fluorescent light or electrodes in the case of sodium lamps) will emit a broad spectrum of light when a continuous symmetrical signal (eg. AC current) is provided to the radiation emitting member.

In typical lighting applications, the provision of visible  
10 light is all that is required. However, the radiation which is emitted by an electron when it changes from one quantum state to another varies depending upon the beginning and end quantum state. Therefore, by controlling the quantum states to which the electrons are raised when excited, the radiation which is produced when an electron reverts to its  
15 normal quantum state may be controlled so as to provide radiation in only a desired portion of the spectrum (eg. visible light in the case of light bulbs).

Accordingly, in accordance with the instant invention, the power control system provides electricity to the radiation emitting  
20 member so as to excite electrons to only specific quantum states. In standard lighting applications, the electric current to the light emitting member preferably would be attenuated so as to produce only or at least more visible light. However, it will be appreciated that in some applications it may be desirable to produce more and preferably only  
25 infrared light, x-rays or another spectrum of radiation.

A power control system for use with, eg., an incandescent light bulb is shown in Figure 7. Commonly, for domestic and industrial applications, voltage source 10 may be an alternating current source, for example a 120 V, 60 Hz supply as used throughout North  
30 America. However, it is equally applicable to a DC source. Electronic control unit 12 is connected to an incandescent light bulb 22, by wires



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storing compounds (reactants) react to produce electrons and unstable products. These products become reactants in subsequent reactions which occur to produce stable products. Each of these reactions proceeds at a different rate. The exact reaction which will occur as well  
 5 as the rates of reactions vary depending on the type of battery which is being used (e.g. an alkaline battery, a lithium battery or a nickel metal hydride battery).

The reactions which occur when a battery is being discharged produce electrons having different potentials. The electrons  
 10 which have a higher potential will result in the production of more electrical power from the power. However, if these higher potential electrons are utilized to complete reactions which may be completed by electrons having a lower potential, then the extra potential will result in the production of work which manifests itself as heat. Currently,  
 15 the standard approach is to discharge a battery by drawing a constant flow of electrons from the battery. The disadvantage of this approach is that the different reactions which occur when a battery is being discharged compete for electrons since each reaction wants to go to completion. Thus, electrons having a higher potential will be used to  
 20 complete reactions which would go to completion by utilizing lower potential electrons.

In accordance to the instant invention, power is withdrawn from a battery in a discontinuous manner so that the reactions are allowed to proceed more toward completion. In this way,  
 25 a greater percentage of the higher potential electrons may be withdrawn from the battery and applied to a load so as to perform work. Further, this reduces the heating of batteries which results in the degradation of secondary batteries. By modulating the electron flow from a battery to preferentially use higher potential electrons to  
 30 provide power to an external load, the actual amount of power which may be withdrawn from a battery may be substantially increased above

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a manufacturer's specification. For example, by using the power control system of the instant invention, a sintered NiMH D cell battery which is designed by a manufacturer to provide 1.2 volts continuously for 6.5 amp hours may be used to provide 1.2 volts for 7.7 amp hours  
5 when pulse train discharging is used.

Therefore, in accordance with this invention, a method for discharging a battery comprises modulating the electron flow from the battery to preferentially use higher potential electrons to provide energy to an external load.

10 Figure 8 shows an apparatus in accordance with the present invention for discharging a battery. Battery holder or connector 32 is shown connected to a pair of batteries or cells 34. It will be understood that, in known manner, either a single battery could be provided or two or more batteries could be provided, connected either  
15 in parallel or in series. Additionally, as already noted, the batteries could be either primary cells or secondary cells.

The battery connector 32 is connected by wires 36 to an electronic control unit 38. This electronic control unit 38 imparts a pulsed wave form to the current drawn from the batteries 34. The  
20 electronic control unit 38 itself takes power necessary for its operation from the batteries 34, but the additional load is minimal, and much less than any power saving achieved.

Figure 8 also shows a second electronic control unit 40 connected by wires 42 to the first electronic control unit 38. This unit is  
25 intended, in this particular embodiment, to further attenuate the signal, to make it suitable for the desired load. For some applications, this second electronic control unit 40 could be omitted. The load for this embodiment is an electric motor, indicated at 44 and connected by wires 46 to the second electronic control unit 40.

30 Conventionally, the motor 44 would simply draw a relatively constant current from the batteries 34. In the present

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invention, the control unit 38 serves to modulate this current drain to give a pulsed wave form. When pulses are provided, it is believed that a relaxation period following each pulse ensures that during each pulse all or most of the charge is drawn at an optimal state. This  
 5 reduces the losses and leads to more efficient recovery of energy stored in the battery or cell.

Conversely, it will be appreciated that the time required to recharge a battery may be substantially reduced by using the power control system of the instant invention. By modulating the electron  
 10 flow to a battery so as to preferentially use lower potential electrons in those reactions requiring only lower potential electrons, the amount of energy which is required to charge a battery is reduced and this consequently decreases the amount of time which is required to recharge the battery. The electron flow which is provided to a battery  
 15 contains electrons at various power levels. When a battery is being recharged, by driving the reactions in reverse and allowing them to proceed more to completion, fewer high potential electrons are required to be input into a system so as to recharge the battery to its desired charge state. Allowing the reaction to proceed more to  
 20 completion, in either direction, decreases the competition for the higher potential electrons. Currently, batteries may be recharged at a rate of up to about  $C/1$  without unduly degrading the battery. At higher rates, excessive heating occurs which will degrade the battery. By using the power control system of the instant invention, a battery may be  
 25 recharged at, for example  $C/0.25$  (ie. for a battery which may be discharged in one hour, the battery may be recharged in 15 minutes).

Therefore, in accordance with this invention, a method for charging a rechargeable battery comprises providing an electrical signal to reverse chemical reactions which occur during the discharge  
 30 of the battery wherein different chemical reactions can utilize electrons having differing potentials and modulating the signal to preferentially

30 In order to demonstrate the power efficiency available using the power control system of the instant invention, a Panasonic motor model number SDS-25IFF was connected downstream from a

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cyclone bin similar to that shown in Figure 5. The air flow rate through the cyclone bin was determined by measuring the pressure drop across the cyclone bin using a manometer. In order to provide a reading of the pressure drop, two pitot tubes were inserted into the air flow path, one upstream of the cyclone bin and the other downstream of the cyclone bin. The pitot tubes provided minimal interaction with the air flow through the air flow conduit. The current and voltage drawn by the motor were measured using a Tektronix A622 AC/DC Current Probe with a frequency response of DC to 100kHz for up to 100A peak current and a Tektronix P5200 High Voltage Differential Probe. The power was calculated by the equation  $P_{elec.inst}(t) = i(t) \cdot v(t)$ . The results are shown in Figure 10. In this Figure, the line designated as "A2" provides the electrical power required by the motor at different flow rates when operated on conventional 60 Hz AC power. The line designated "A" is the electrical power required to obtain the same flow rates using the power control system of the instant invention. The signal which is fed to the motor is shown in Figure 12(a). As shown in Figure 12(a), the pulse train had a frequency of 12.5Hz (i.e. each cycle or pulse train had a duration of 80 milliseconds) with 10 pulses per cycle. The strongest pulse (pulse C) had a peak voltage of about 120 volts. The peak pulse was sandwiched between two strong pulses (pulses B) which had a peak voltage of about 60 volts. The remaining pulses (pulses A) had a peak voltage of about 20 volts. Two other signals on which the motor was operated are shown in Figures 12(b) and (c). The signal shown in Figure 12(b) had a peak voltage for pulse A of 106 volts. The pulse train had a frequency of 13 Hz. The signal shown in Figure 12(c) had a peak voltage for pulse A of 90 volts. The pulse train had a frequency of 9 Hz.

A second test was conducted utilizing a custom wound 50 volt test motor which was obtained from Amatek (model number E-11459-2D). The results are set out in Figure 11. Once again, line "A2" is



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used to designate the power required when the motor was operated on conventional 60 Hz DC power and line "A" is used for the line representing the power required when the motor was operated using the power control system of the instant invention. In this case, the signal fed to the motor was similar to that fed to the Panasonic motor.

### Example 2

This Example demonstrates the use of a pulsed train signal with a light bulb. As shown in Figure 13, a pulse train wherein each period contained five pulses was fed to a light bulb.

Within the period or cycle 220, there are five pulses, indicated at 221, 222, 223, 224, and 225. The pulses are spaced by intervals indicated as  $\lambda_1$ ,  $\lambda_2$ ,  $\lambda_3$ ,  $\lambda_4$ ,  $\lambda_5$ . The specific values for these pulses in this example are:

Pulse No.	Voltage	Duration of Pulse (Pulse Width)	Pulse Interval
21	50	10	$\lambda_1=10$
22	55	7	$\lambda_2=12$
23	60	12	$\lambda_3=8$
24	57	9	$\lambda_4=10$
25	48	9	$\lambda_5=12$

As indicated at the right hand side, at 221', the next period has the same sequence of pulses.

As this table shows, within the period 220, all the parameters of the pulses, namely frequency (i.e. inverse of the pulse interval), pulse width or duration, and pulse height (voltage) are varied. This gives a distinct pulse profile for the period, and this is repeated in following periods. In general, depending on the particular application, it may

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not be necessary to vary all three parameters, and it may be sufficient to vary just two of them, or even just one of them, with the other(s) being kept constant. Additionally, it will be understood that the absolute magnitude of each of these parameters can vary greatly depending upon the actual application.

It is believed that by selection of suitable parameters, a resonance effect is achieved, causing the filament to provide a significantly larger proportion of the radiation in the visible region. This enables, for example, a normally 40-watt bulb to be driven with significantly less than 40 watts of power, and yet still produce the same amount of visible light.

Figure 14 shows a print out of a pulsed signal which was used for a fluorescent light bulb. As can be seen from Figure 14, the voltage which was applied to the light bulb was relatively constant. However, the current fluctuated substantially and comprised a signal having 10 pulses per period. Each cycle or period was 1/9 second and the frequency was 9 Hz. A light meter was used to measure the visible light emitted by the light bulb when the light bulb was operated on a standard AC signal and when the light bulb was operated on the signal of Figure 14. When the signal of Figure 14 was used, the light bulb emitted the same amount of visible light but consumed 18% less power.

### Example 3

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A pulsed signal comprising ten pulses per period was provided to a secondary battery for recharging the battery. The pulse train was similar to that shown in Figure 12. In this case, peak voltage "C" was 21 volts, pulse B was 16.5 volts and the remaining pulses (pulses A) had a peak voltage of 14.5 volts. The duration of each pulse was 0.1 seconds. As a result of this pulse train, sub-C batteries were charged at a

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rate of  $C/_{0.5}$  (i.e. they were charged in 30 minutes) without causing any heat damage to the batteries.

- ART 34 AMDT
1. A method of controlling the electrical power applied to a load, the method comprising the steps of:
    - (a) producing a pulse train comprising a series of pulses having at least two pulses which differ in voltage and/or polarity and defining a cycle in which a portion of the pulse train having a duration of 10% of the cycle delivers more than 20% of the total power to the load which the load receives each cycle; and,
    - (b) supplying the pulse train to the load to supply power to the load.
  2. The method as claimed in claim 1 wherein the pulses are varied so that at least two of the pulses deliver differing amounts of power to the load.
  3. The method as claimed in claim 1 further comprising the step of providing a first electrical signal to the load and periodically superimposing a second signal to the load whereby the load periodically receives a pulse at a higher voltage than the first electrical signal.
  4. The method as claimed in claim 1 further comprising the step of providing an electric power supply and the pulse train is produced by modulating the electric power supply to produce the pulse train.
  5. The method as claimed in claim 1 wherein the portion provides 30 - 70% of the total power the load receives each second.
  6. The method as claimed in claim 1 wherein the portion provides 40 - 60% of the total power the load receives each second.
  7. The method as claimed in claim 1 wherein the portion provides 45 - 55% of the total power the load receives each second.
  8. The method as claimed in claim 1 wherein the cycle has a frequency of 6 - 20Hz.
  9. The method as claimed in claim 1 wherein the cycle has a frequency of 9 - 15Hz.

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- ART 34 ANDT
10. The method as claimed in claim 1 wherein each cycle comprises 1 - 20 pulses.
  11. The method as claimed in claim 1 wherein each cycle comprises 5 - 15 pulses.
  12. The method as claimed in claim 1 wherein the signal is non-uniform.
  13. The method as claimed in claim 1 wherein the load comprises a motor and impact member assembly and the pulse train is modulated to vary the acceleration of the impact member to reduce degradation of a Prandtl layer which forms on the impact member as the fluid travels over the impact member.
  14. The method as claimed in claim 1 wherein the load comprises a radiation emitting device having a radiation emitting member which emits radiation in a plurality of bands when a uniform electrical signal is provided to the radiation emitting member and the pulse train is modulated to excite electrons to selected quantum states to preferentially produce radiation in a selected spectrum.
  15. The method as claimed in claim 1 wherein the load comprises a member selected from the group consisting of a fluorescent light bulb and a sodium lamp and the pulse train is modulated to excite electrons to selected quantum states to preferentially produce light.
  16. The method as claimed in claim 1 wherein the load comprises a rechargeable battery in which, during the discharge of the battery, chemical reactions occur that can utilize electrons having differing potentials and during recharging, the chemical reactions are reversed and the pulse train is modulated to preferentially use electrons having a higher potential to reverse chemical reactions requiring higher potential electrons.
  17. The method as claimed in claim 1 wherein the load comprises a rechargeable battery in which, during the discharge of the battery, chemical reactions occur that can utilize electrons having differing potentials and during discharging the pulse train is modulated to preferentially use higher potential electrons to provide energy to an

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ART 34 AMDT  
external load.

18. A method of controlling the mechanical power applied to a load, the method comprising the steps of:

- (a) producing changes in the acceleration of a mechanical member whereby a series of differing accelerations are applied in a repeating pattern to produce the mechanical power, a portion of the series having a duration of 10% of the pattern delivers more than 20% of the total power to the load which the load receives during the repetition of each period; and,
- (b) supplying the mechanical power to the load to supply mechanical power to the load.

19. The method as claimed in claim 18 wherein the load comprises an impact member and the mechanical power is modulated to reduce degradation of a Prandtl layer which forms on the Prandtl layer as fluid travels over the impact member.

20. The method as claimed in claim 18 wherein the mechanical member comprises an impact member and the mechanical power is modulated to reduce degradation of a Prandtl layer which forms on the Prandtl layer as fluid travels over the impact member.

21. The method as claimed in claim 18 wherein the portion provides 30-70% of the total power the load receives each second.

22. The method as claimed in claim 18 wherein each period comprises 1-20 differing accelerations.

23. The method as claimed in claim 18 wherein each period comprises 5-20 differing accelerations.

24. The method as claimed in claim 18 wherein the rate of rotation of the impact member is varied a plurality of times during each revolution of the impact member whereby the rate of rotation of the impact member is non-uniform.

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(b) varying the rate of rotation of the impact member to reduce the degradation of the Prandtl layer as the fluid travels over the impact member.

26. The method as claimed in claim 25 wherein the impact member comprises the power transfer member of a fluid pump and the method further comprises driving the impact member to cause the fluid to flow.

(b) varying the rate of rotation of the impact member to reduce the degradation of the Prandtl layer as the fluid travels over the impact member.

28. The method as claimed in claim 27 wherein the apparatus comprises an electrical generator and the method further comprises driving the generator to produce electrical current.

29. The method as claimed in claim 27 wherein the apparatus comprises a drive rod and the method further comprises driving the drive rod with the impact member to obtain mechanical power.

(a) providing a power supply to produce a signal to excite selected quantum states within the radiation emitting member to preferentially produce radiation

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in a selected spectrum; and,

(b) supplying the signal to the radiation emitting device to supply power to the radiation emitting member.

31. The method as claimed in claim 30 wherein the radiation emitting member comprises an incandescent light bulb and the radiation emitting member comprises a filament and the method comprises producing a signal to preferentially produce radiation in the visible spectra.

32. The method as claimed in claim 30 wherein the radiation emitting member comprises an fluorescent light bulb and the radiation emitting member comprises gas in the fluorescent light bulb and the method comprises producing a signal to preferentially produce radiation in the visible spectra.

33. The method as claimed in claim 30 wherein the radiation emitting member comprises a sodium lamp and the radiation emitting member comprises electrodes and the method comprises producing a signal to preferentially produce radiation in the visible spectra.

34. The method as claimed in claim 30 wherein the method comprises producing a signal to preferentially produce infrared radiation.

35. The method as claimed in claim 30 wherein the method comprises producing a signal to preferentially produce x-ray radiation.

36. A method for discharging a battery comprising modulating the electron flow from the battery to preferentially use higher potential electrons to provide energy to an external load.

37. A method for charging a rechargeable battery comprising providing an electrical signal to reverse chemical reactions which occur during the discharge of the battery wherein different chemical reactions can utilize electrons having differing potentials and modulating the signal to preferentially use electrons having a higher potential to

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8 November 2001

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**WO 01/29950 A3**

**(54) Title:** METHOD AND APPARATUS FOR DELIVERING POWER TO A MECHANICAL OR ELECTRICAL SYSTEM

**(57) Abstract:** A power control system for use in providing mechanical or electrical power to a load is used to operate a system to provide a series of pulses to the system wherein the pulses within each series provide differing amounts of power. Preferably, a portion of the series which has a duration of 10 % of the cycle delivers more than 20 % of the total power to the load which the load receives each cycle.

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Figure 1A

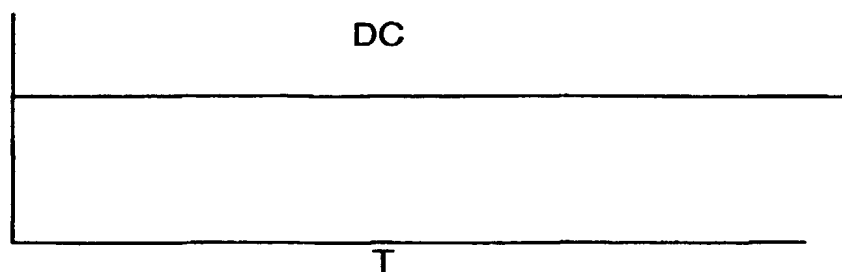


Figure 1B

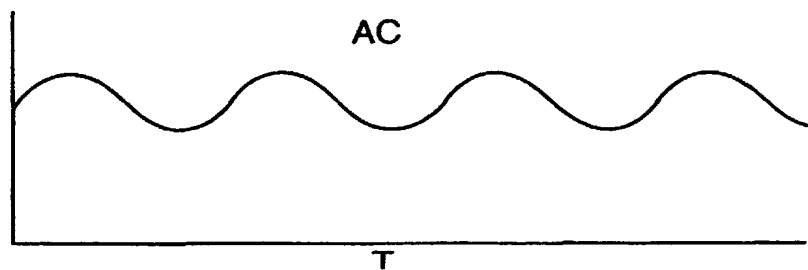


Figure 1C

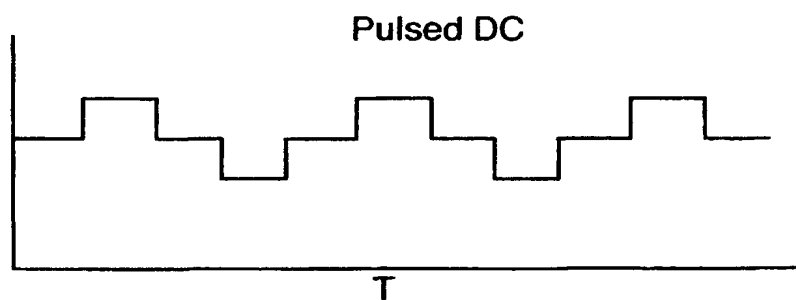


Figure 1D

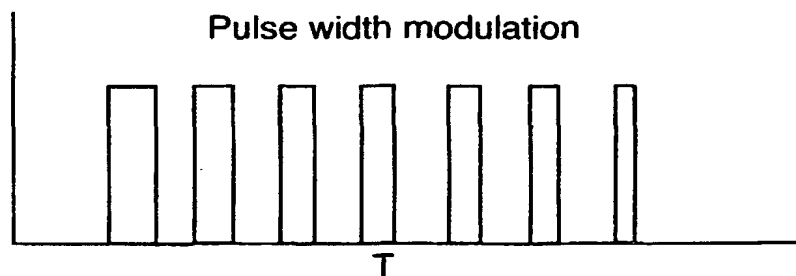


Figure 1E

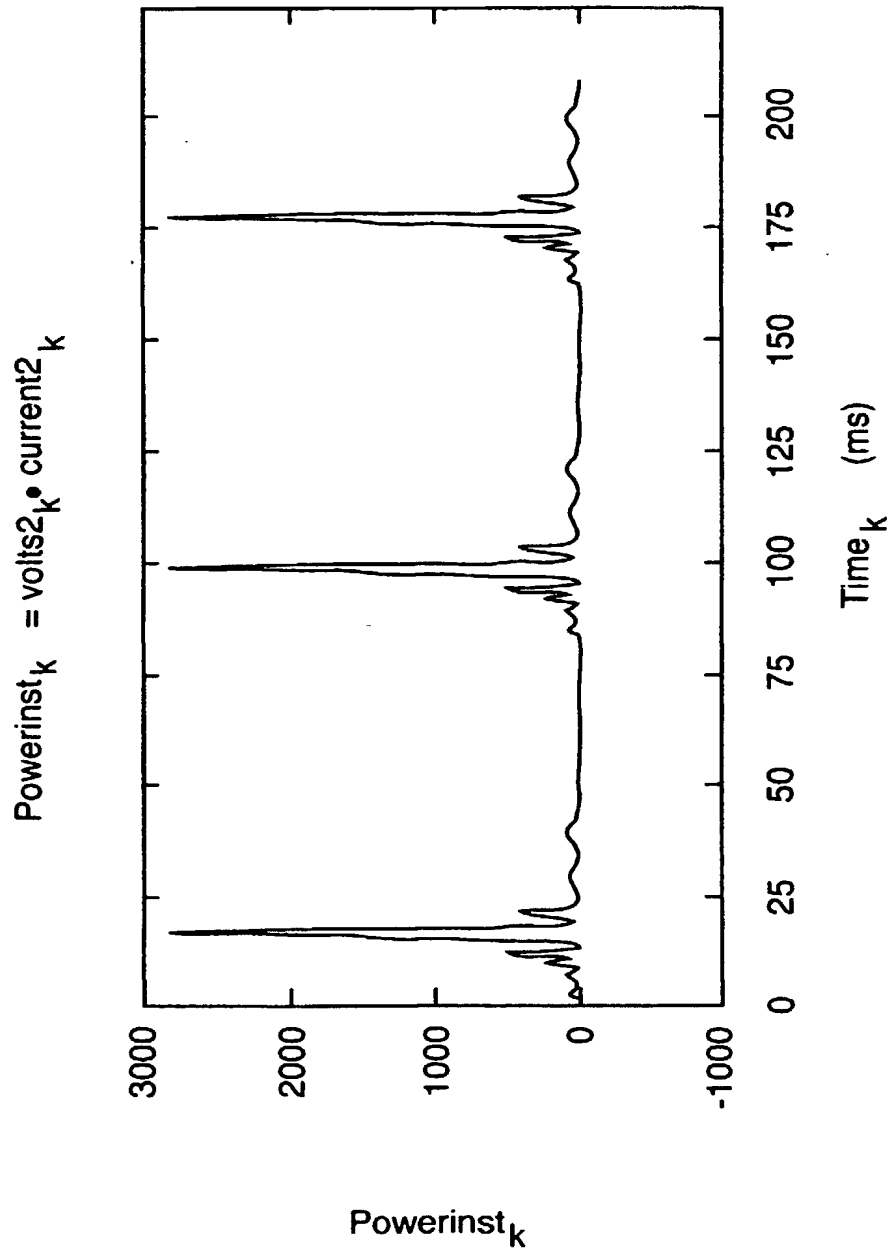
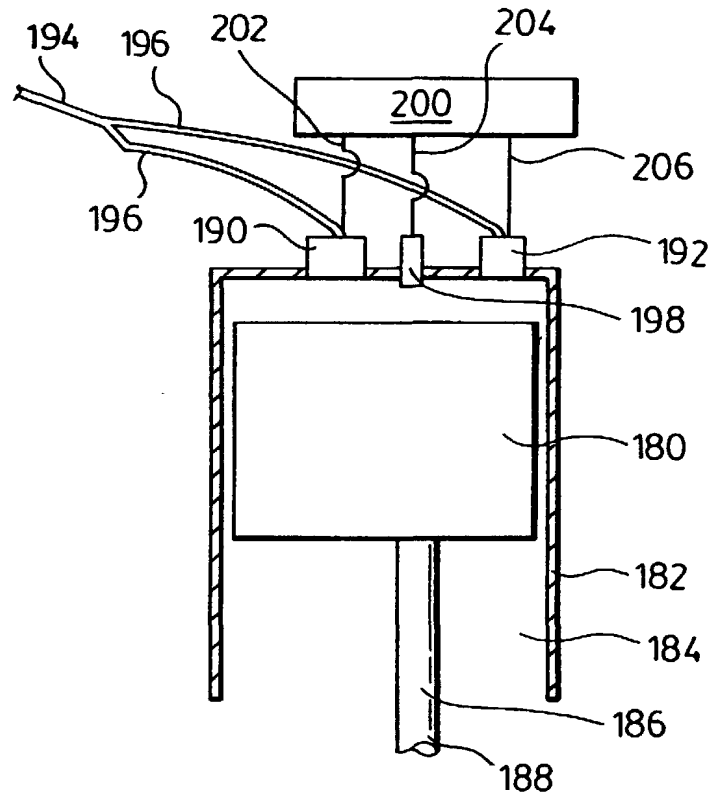
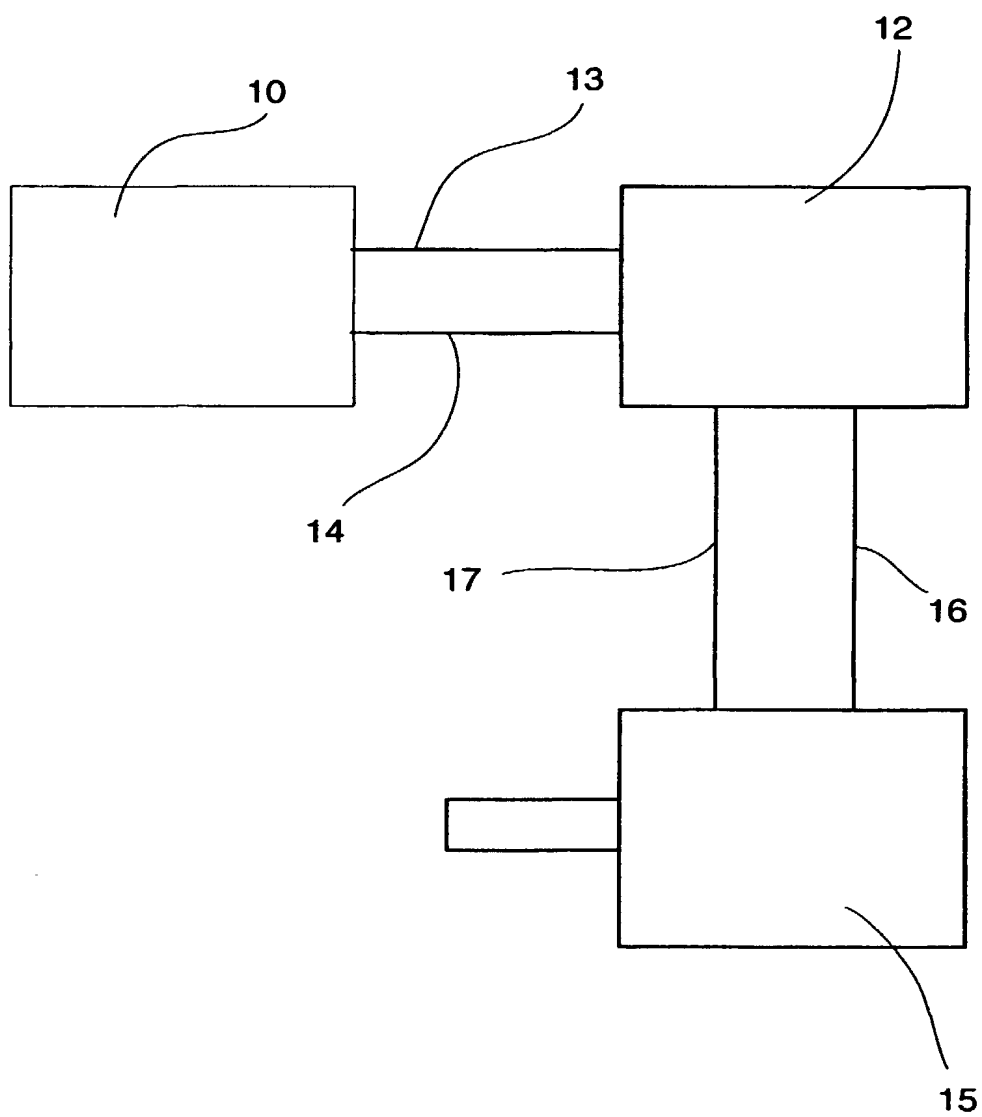


Figure 2



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Figure 3



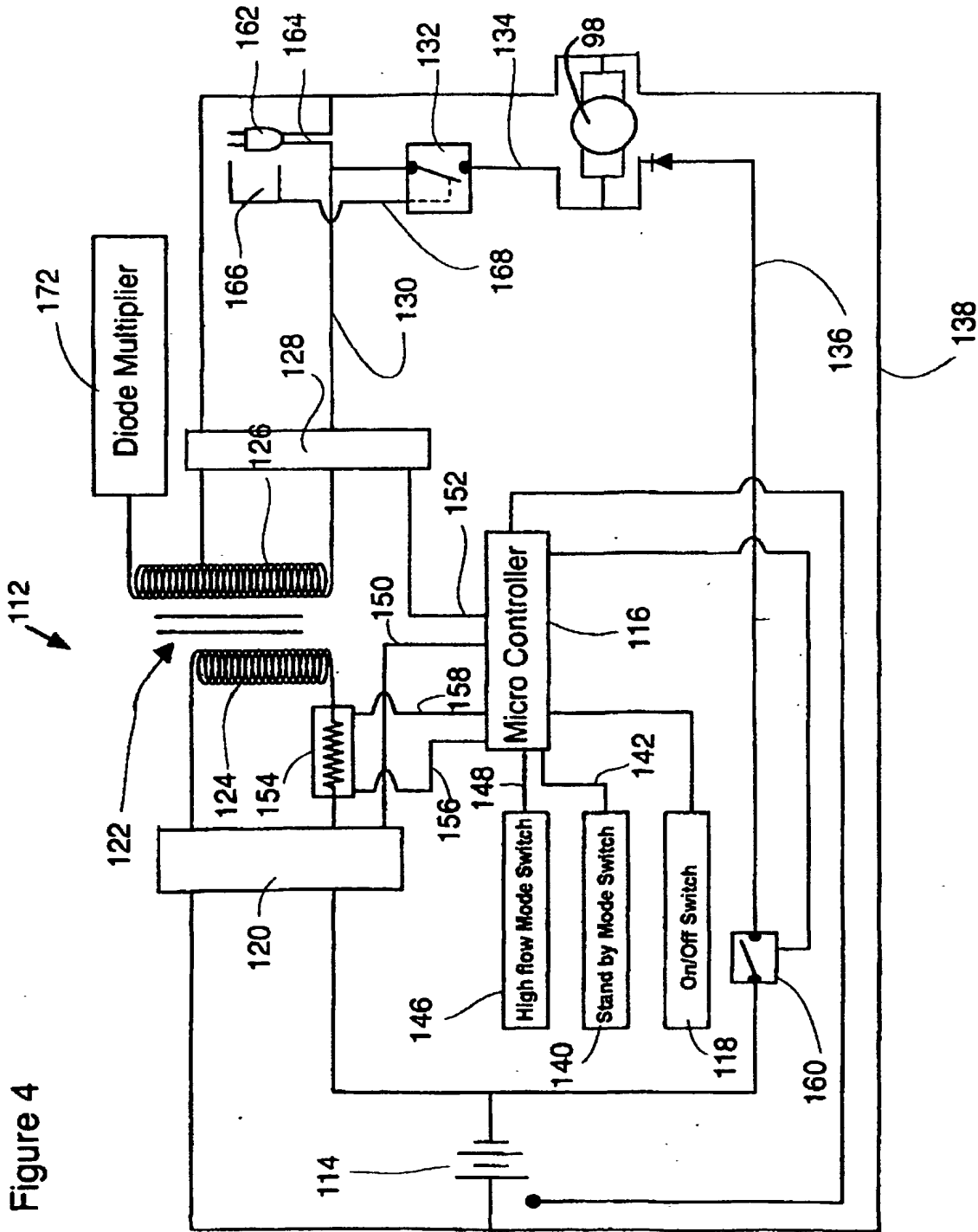
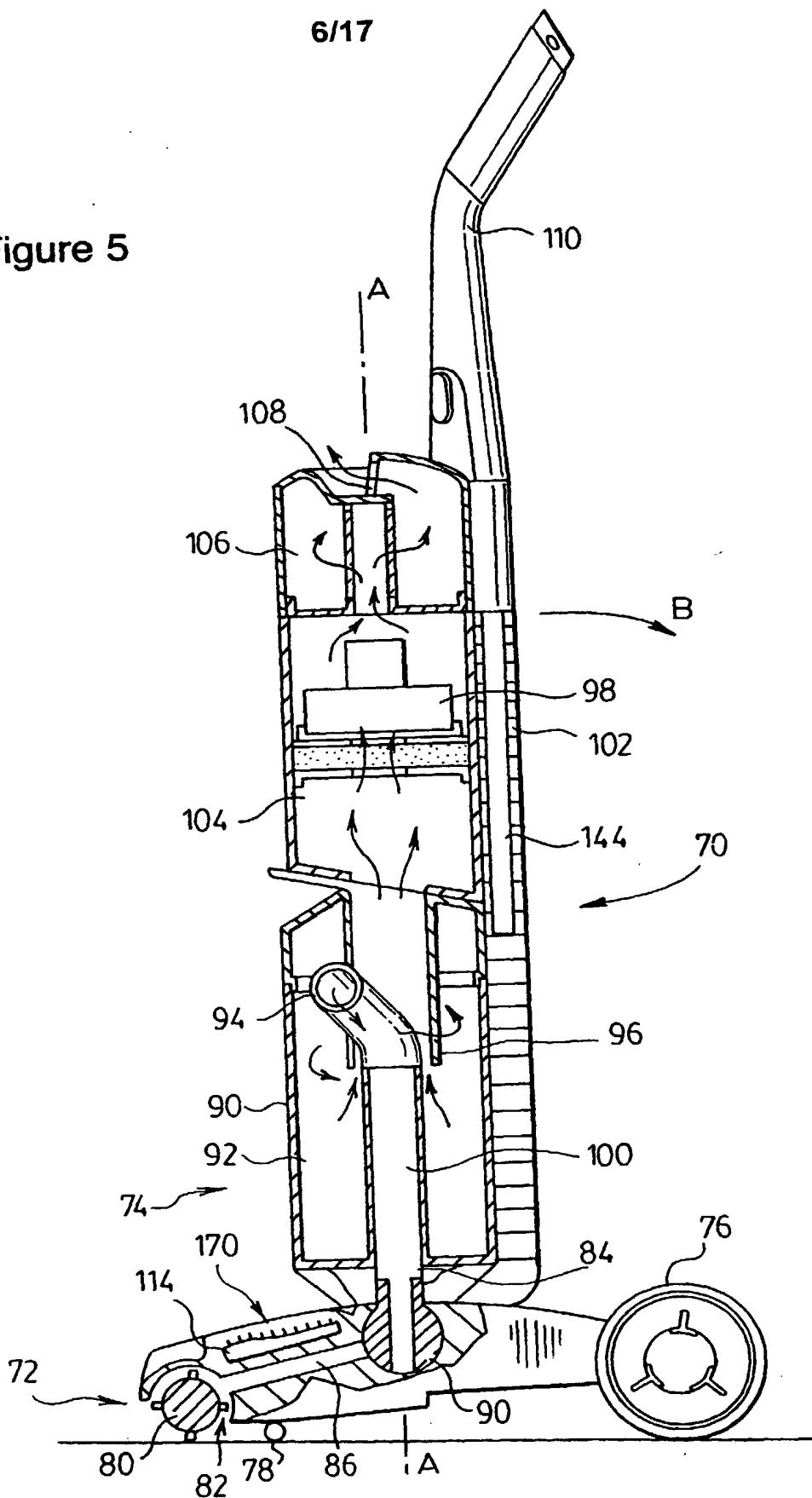


Figure 4

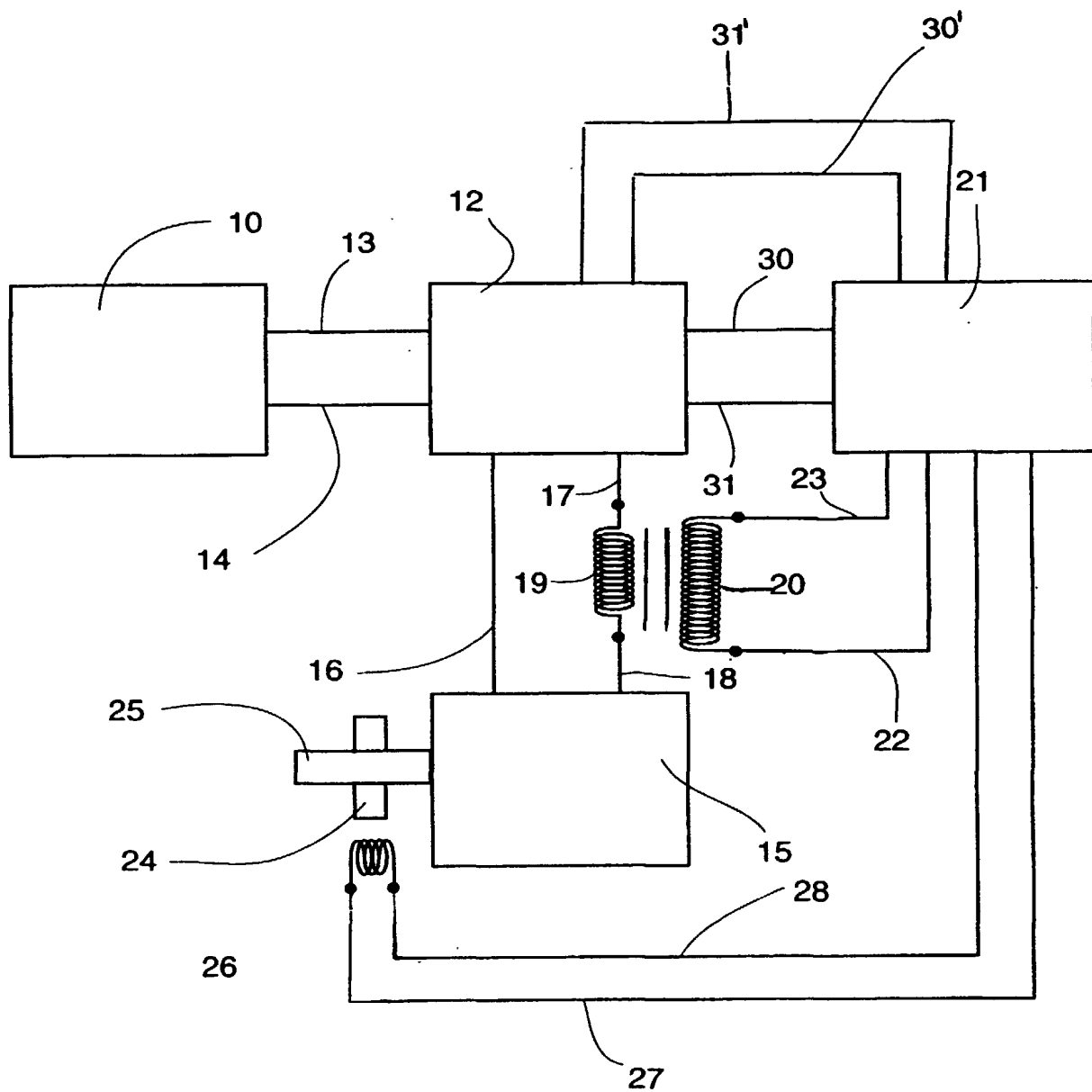
Figure 5





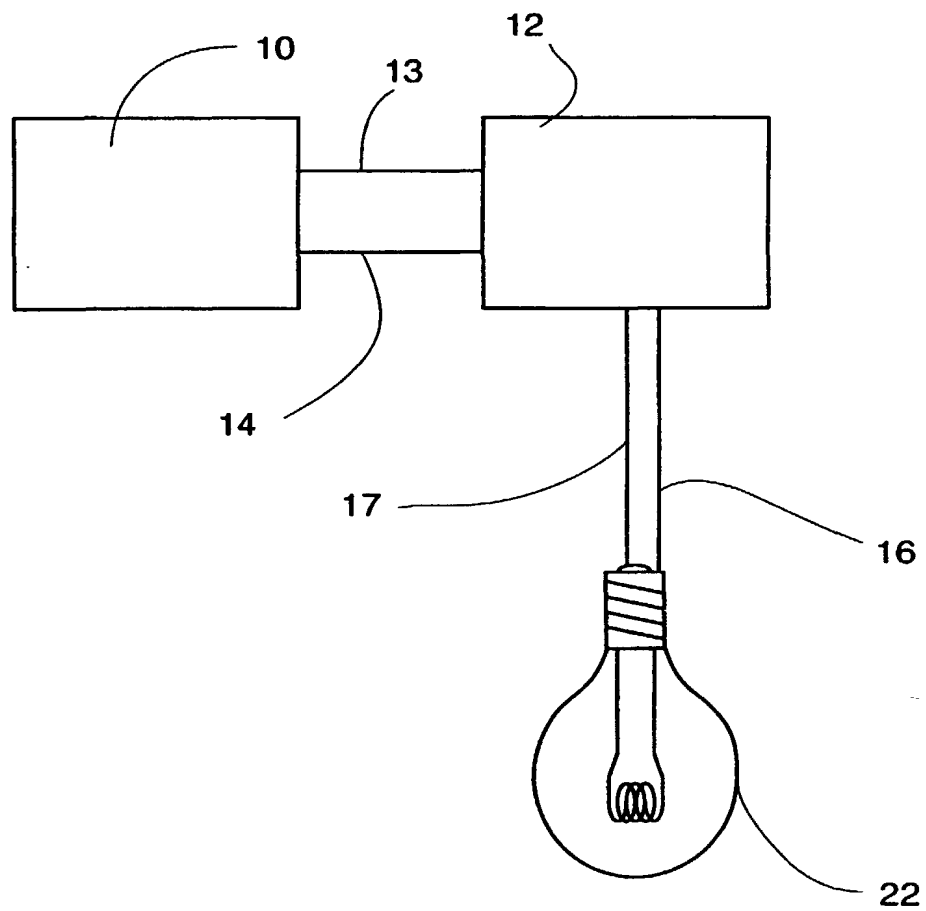
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Figure 6



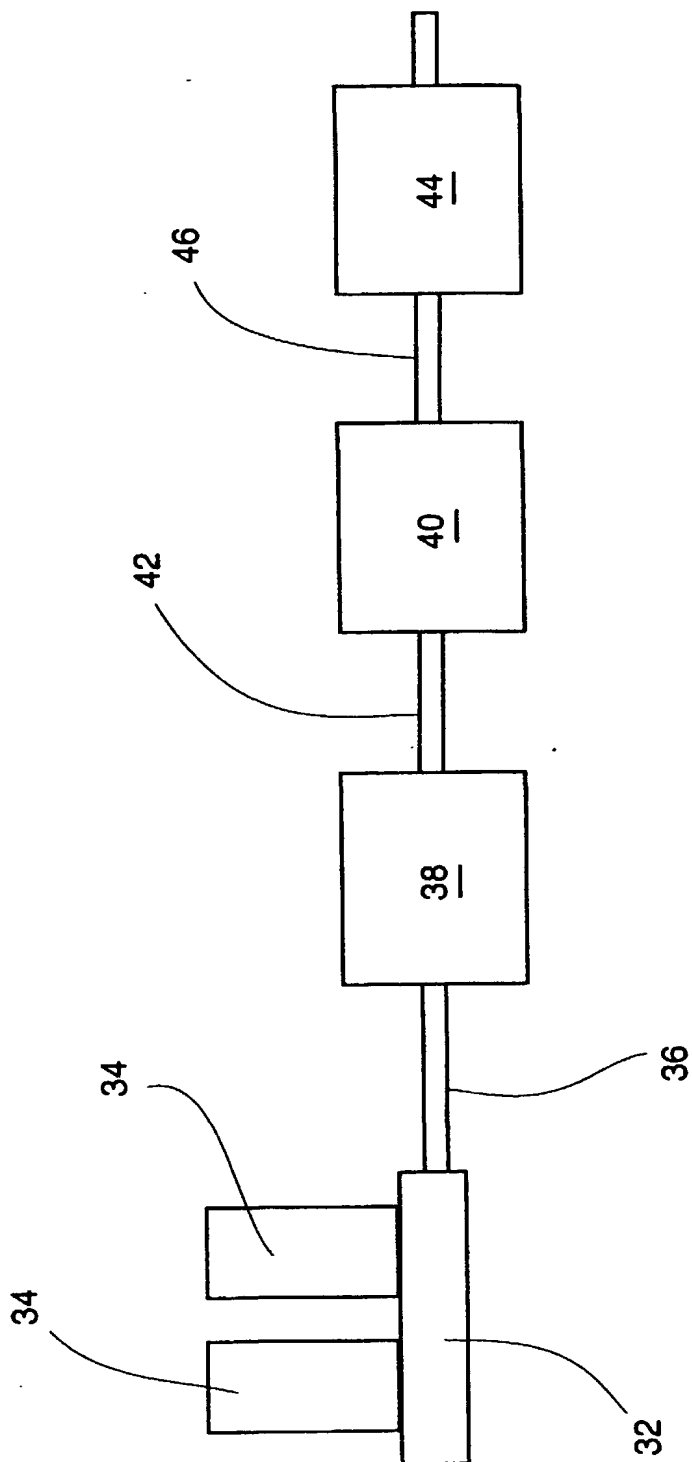
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Figure 7



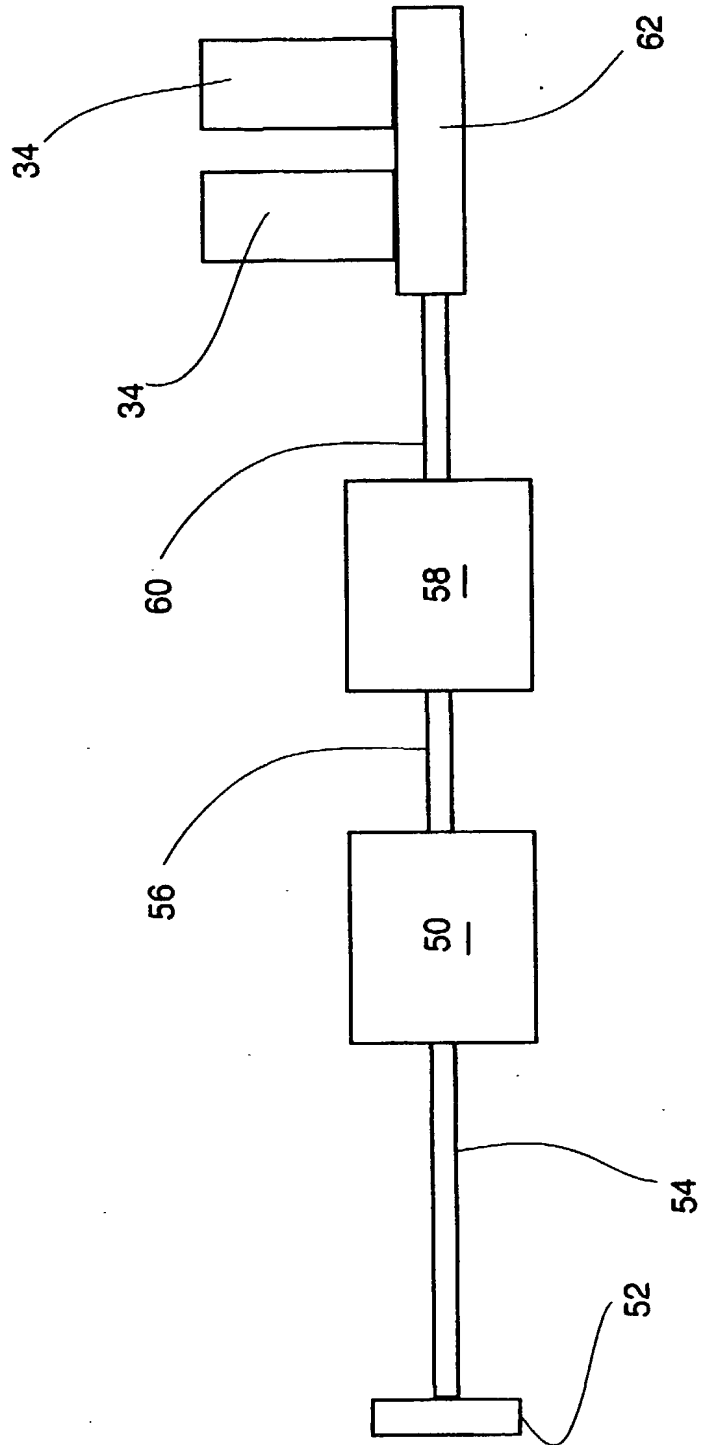
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Figure 8



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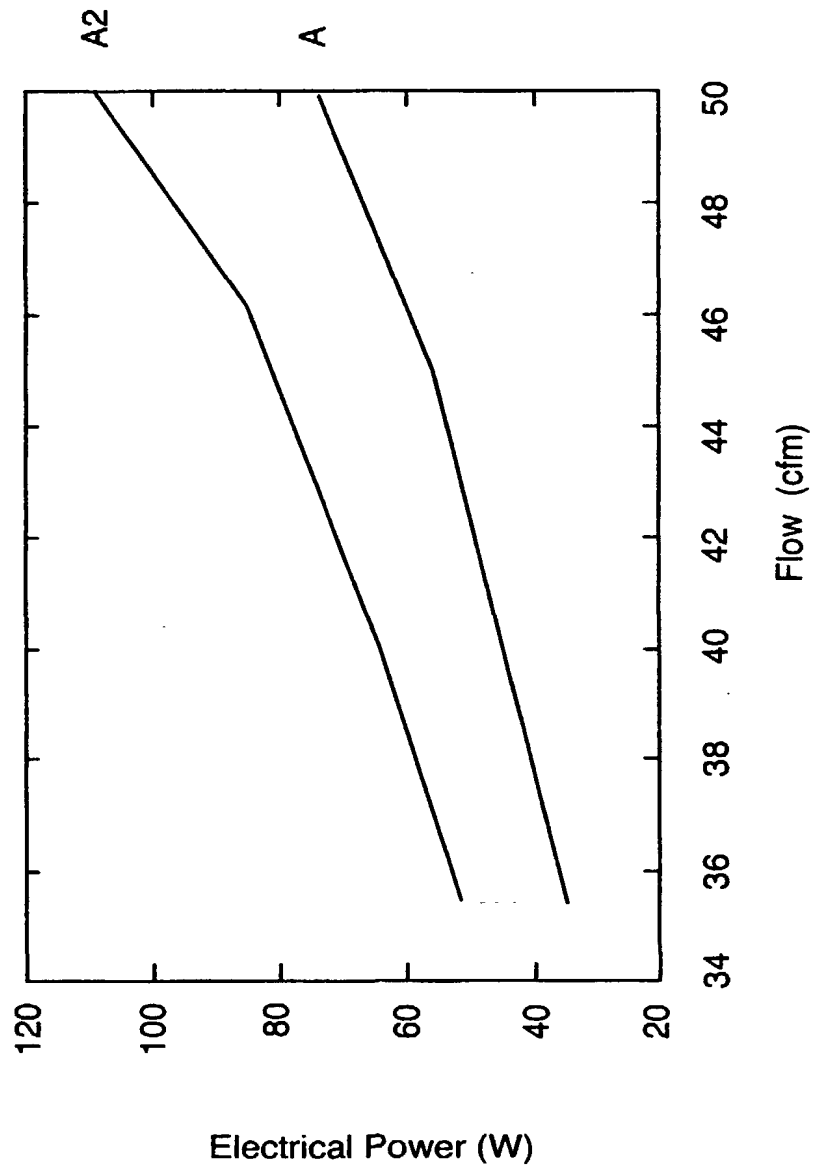
Figure 9



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Figure 10

ElectPower vs Flow



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Figure 11

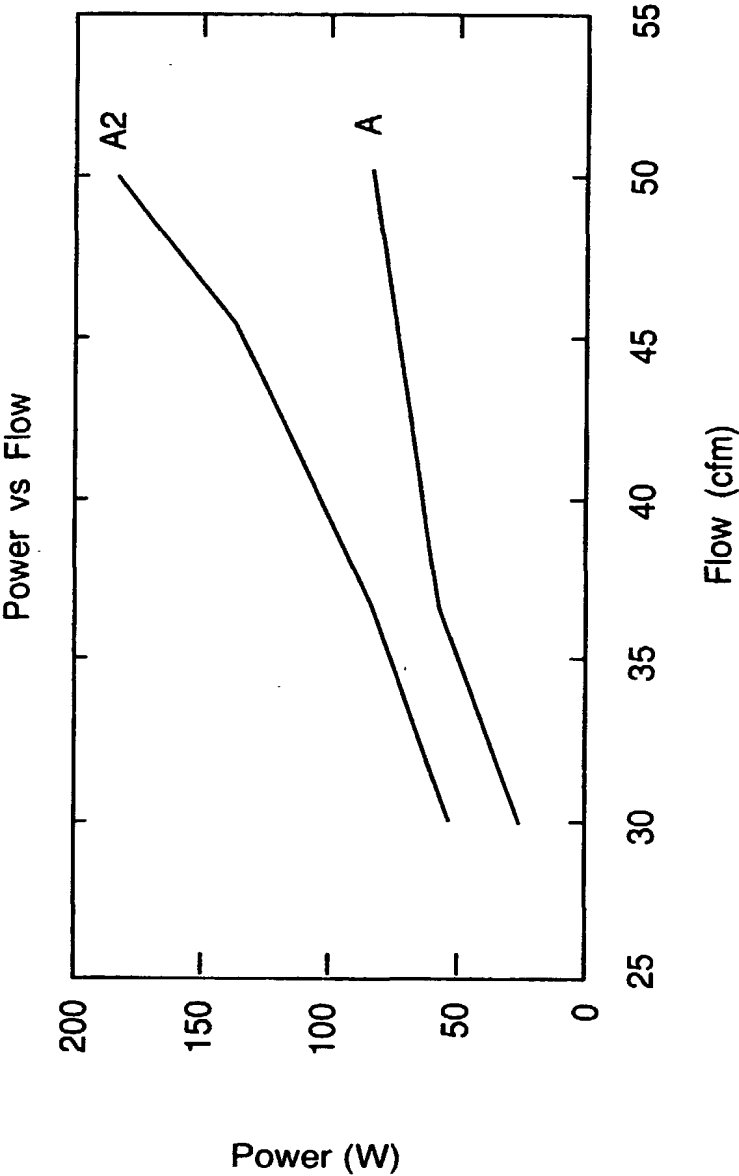
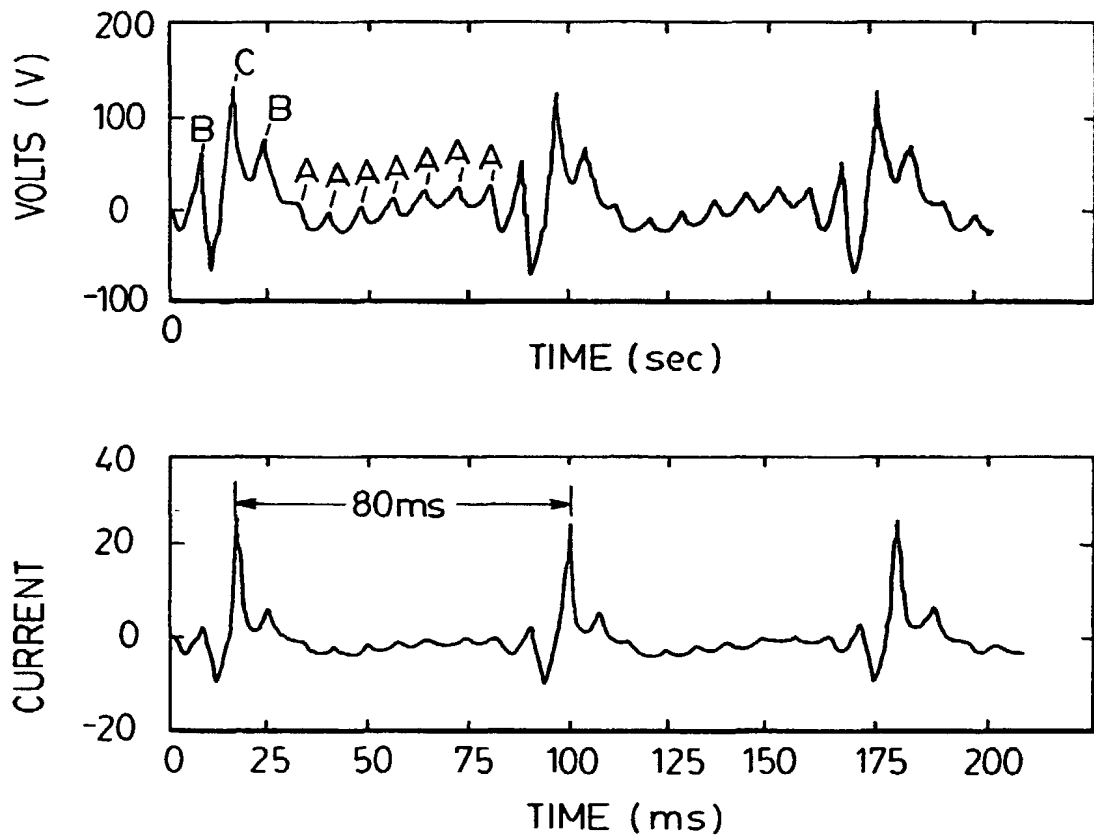


Figure 12A



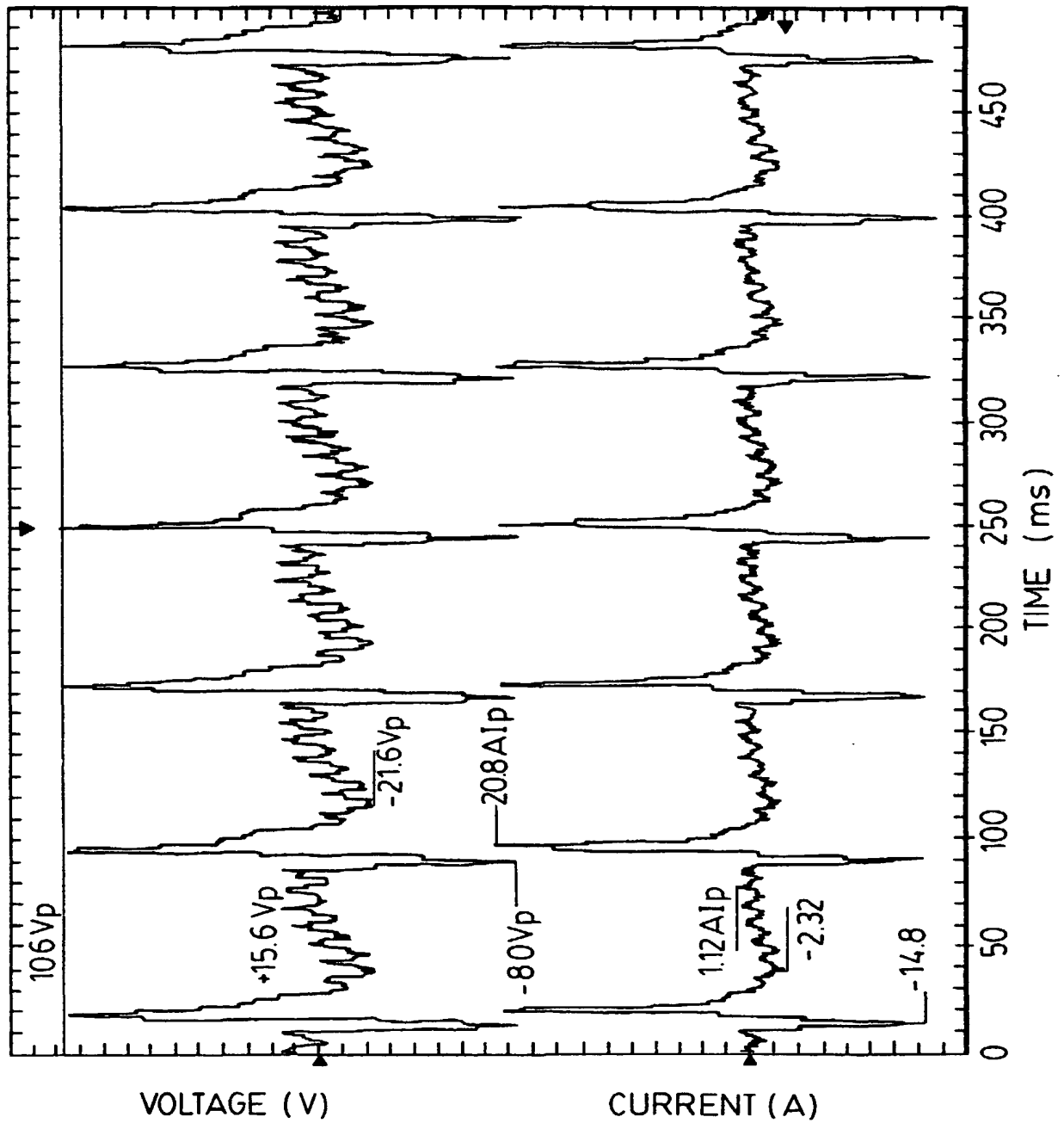


Figure 12B



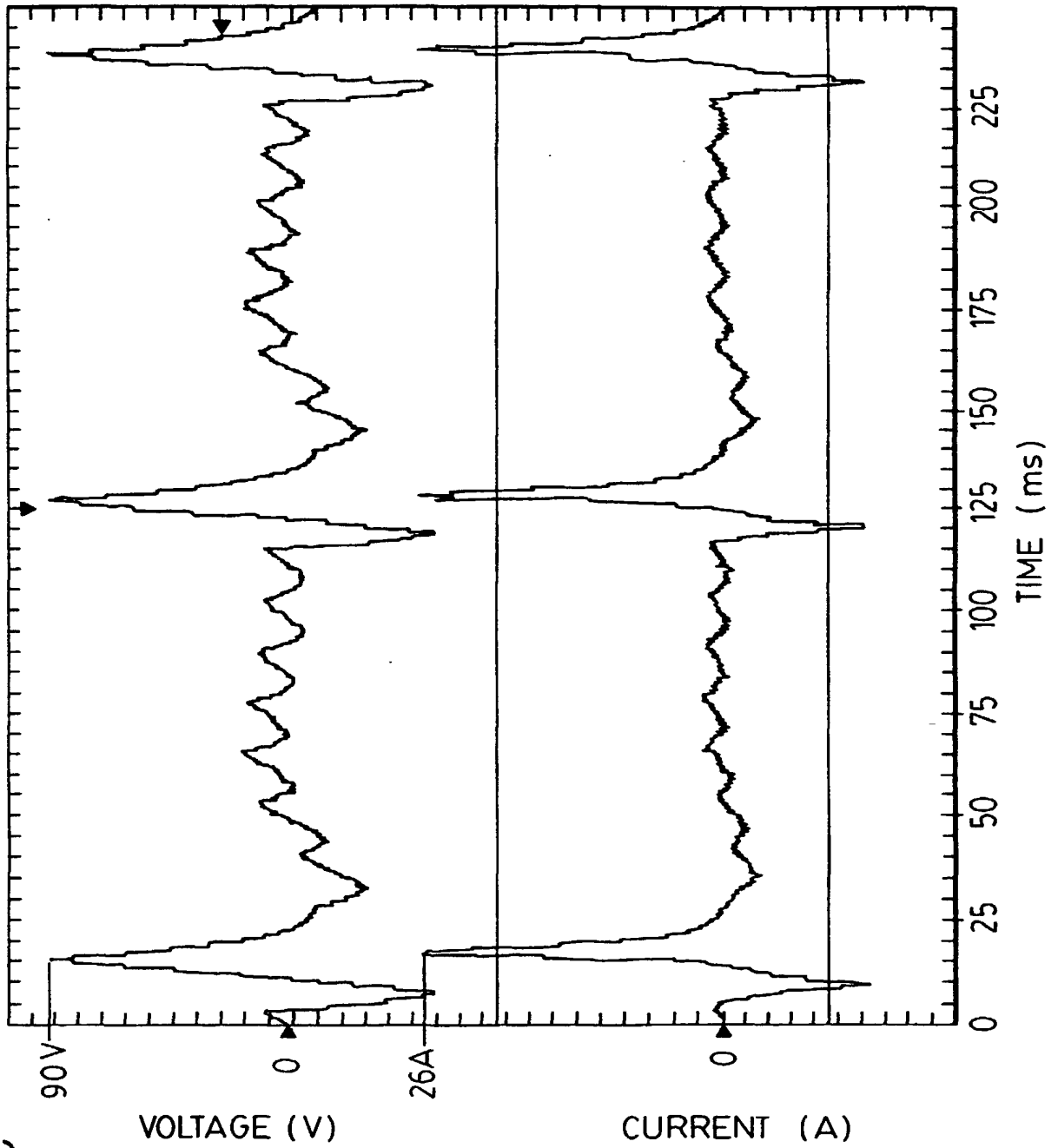
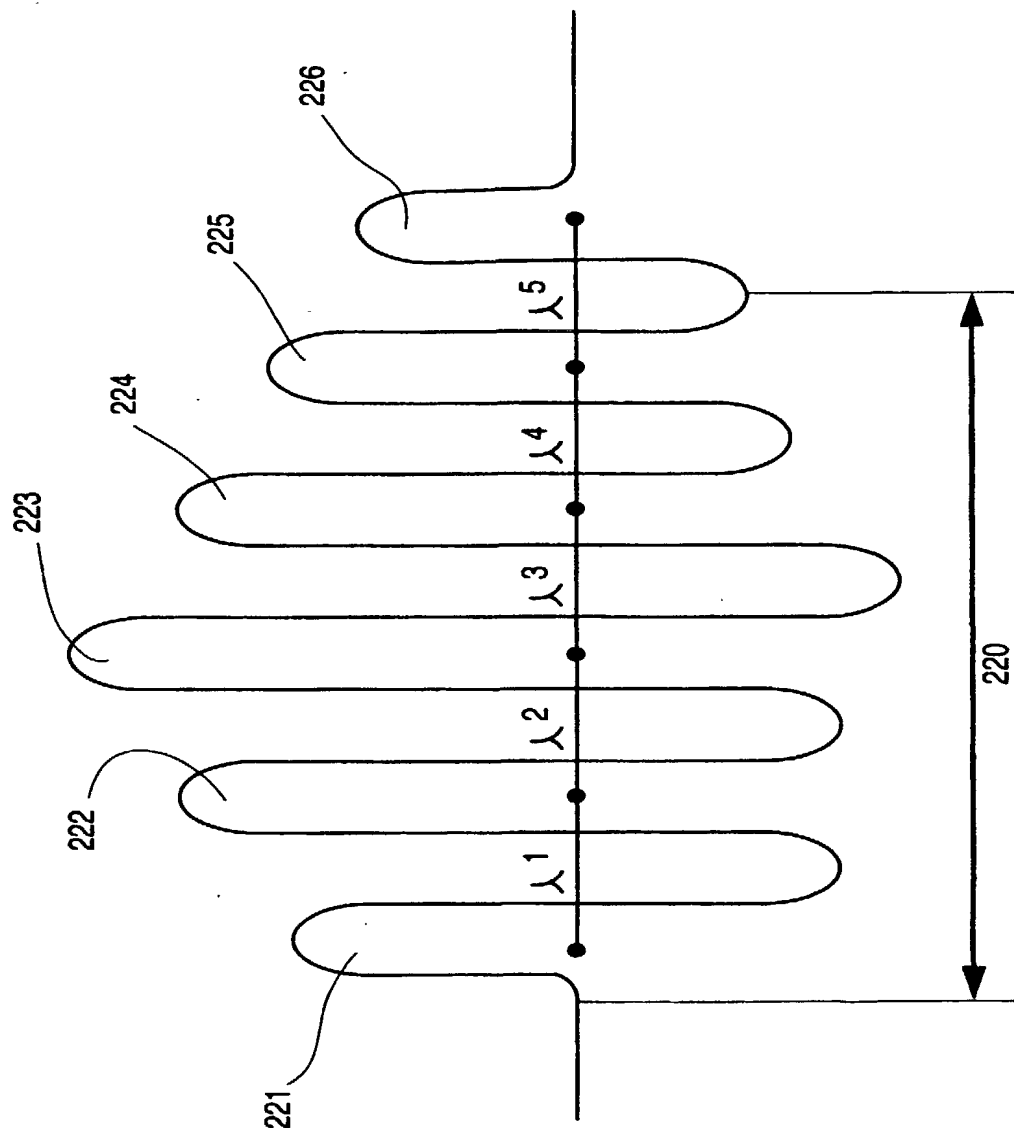


Figure 12C

Figure 13



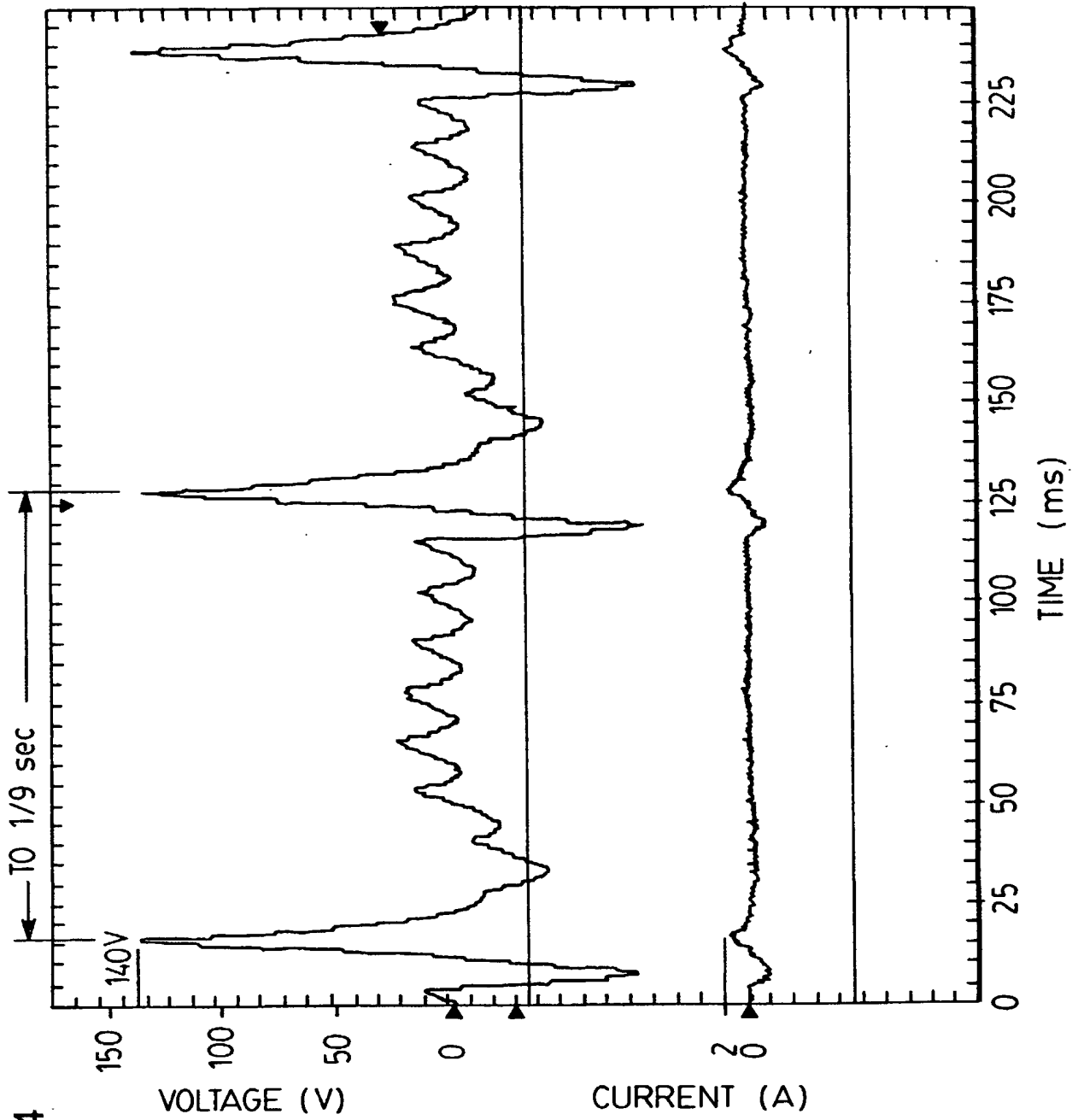


Figure 14

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	<b>First Named Inventor</b>	Conrad
	<b>COMPLETE IF KNOWN</b>	
	<b>Application Number</b>	10/089,100
	<b>Filing Date</b>	October 13, 2000
	<b>Group Art Unit</b>	n/a
	<b>Examiner Name</b>	n/a

As a below named inventor, I hereby declare that:

My residence, post office address, and citizenship are as stated below next to my name.

I believe I am the original and first inventor of the subject matter which is claimed and for which a patent is sought on the invention entitled:

METHOD AND APPARATUS FOR DELIVERING POWER TO A MECHANICAL OR ELECTRICAL SYSTEM

the specification of which (Title of the Invention)

☐ is attached hereto

OR

☐ was filed on (MM/DD/YYYY) October 13, 2000 as United States Application Number or PCT International

Application Number 10/089,100 and was amended on (MM/DD/YYYY)  (if applicable)

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims as amended specifically referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR 1.56, including for continuation-in-part applications, material information which became available between the filing date of the prior application and the national or PCT international filing date of the continuation-in-part application


I hereby claim foreign priority benefits under 35 U.S.C. 119(a)-(d) or (f), or 365(b) of any foreign application(s) for patent, inventor's or plant breeder's rights certificate(s), or 365(a) of any PCT international application which designated at least one country other than the United States of America, listed below and have also identified below, by checking the box any foreign application(s) for patent, inventor's or plant breeder's rights certificate(s), or of any PCT international application having a filing date before that of the application on which priority is claimed.

Prior Foreign Application Number(s)	Country	Foreign Filing Date (MM/DD/YYYY) Country	Priority Not Claimed	Certified Copy Attached?	
				YES	NO
2,286,883	Canada	October 15, 1999	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
			<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
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			<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

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[Page 1 of 2]

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I hereby claim the benefit under 35 U.S.C. 120 of any United States application(s), or 365(c) of any PCT international application designating the United States of America, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT international application in the manner provided by the first paragraph of 35 U.S.C. 112, I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR 1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application.

U.S. Parent Application or PCT Parent Number	Parent Filing Date (MM/DD/YYYY)	Parent Patent Number (if applicable)
PCT/CA00/01183 US Patent Appl. No. 09/557,223	Oct. 13, 2000 Apr. 25, 2000	6,307,358

☐ Additional U.S. or PCT international application numbers are listed on a supplemental priority data sheet PTO/SB/02A attached hereto.

As a named inventor, I hereby appoint the following registered practitioner(s) to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith: ☒ Customer Number 1059 OR ☐ Registered practitioner(s) name/registration number listed below.

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Richard J. Parr	22,836	Philip Mendes da Costa	33,106
H. Roger Hart	26,426	Robert B. Storey	33,108
David W.R. Langton	27,747	John R. Rudolph	38,003
C. Lloyd Sarginson	29,245	Robin L.A. Coster	38,016
Timothy J. Sinnott	31,083	Michael E. Charles	38,036

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Name of Sole or First Inventor: WAYNE ERNEST ☐ A petition has been filed for this unsigned inventor

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Country	Canada				

☐ Additional inventors are being named on the supplemental Additional Inventor(s) sheet(s) PTO/SB/02A attached hereto